

MODEL 431B<br>SERIALS PREFIXED: 233-

## POWER METER



ISOI PAGE MILI ROAD. PAIO ALIO. CALIFORNIA, U.S.A.

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Figure 1-1. Model 431B Power Meter

## SECTION I GENERAL INFORMATION

## 1-1. DESCRIPTION.

1-2. The ( 10 Model 431B Power Meter, with (tip temperature compensated thermistor mounts, measures rf power from 10 microwatts ( -20 dbm ) to 10 milliwatts ( +10 dbm ) in the $10-\mathrm{mc}$ to $40-\mathrm{gc}$ frequency range. Direct reading accuracy of the instrument is $\pm 3 \%$ of full scale. Instrument specifications are given in table 1-1.

1-3. The design of the Model 431B and its thermistor mount, results in almost complete freedom from measurement error caused by ambient temperature changes. The instrument incorporates two selfbalancing bridges with one arm of each bridge being a thermistor. The two matched thermistors, both located within the mount, are thermally coupled, but
electrically isolated. One thermistor is used to absorb rf power; the other is used to provide temperature compensation. Thus, the thermal drift problems normally associated with the thermistor-power meter arrangement have been greatly reduced. A single setting of the ZERO control on the most sensitive power range is maintained within $1 \%$ for all higher power ranges.

1-4. The temperature compensated thermistor mounts used with the instrument are specifically designed for (4) Model 431A/B Power Meters. Coaxial and waveguide thermistor mounts cover the $10-\mathrm{mc}$ to $40-\mathrm{gc}$ frequency range. Table 1-2 gives thermistor mount operating frequency, mount configuration, and operating resistance.

Table 1-1. Specifications

## Instrument Type:

Automatic, self-balancing for temperature compensated mounts

## Power Ranges:

7 ranges with full scale readings of $10,30,100$ and $300 \mu \mathrm{w}$; 1, 3 and 10 mw . Also calibrated in dbm from -20 to +10 .

External Bolometer:
Temperature-compensated thermistor mounts required for operation (62) 478A and 486A series).

## Accuracy:

$\pm 3 \%$ of full scale from $+20^{\circ} \mathrm{C}$ to $+35^{\circ} \mathrm{C}, \pm 5 \%$ of full
scale from $0^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$

## Zero Carry-Over:

Less than $1 \%$ of full scale when zeroed on most sensitive range

Recorder/Voltmeter Output:
Phone jack on rear with 1 ma maximum into 1000 ohms $\pm 10 \%$; one side grounded

Calibration Input:
Binding posts on rear for calibration of bridge with (40) 8402A Power Meter Calibrator or precise dc standards

Power Supply:
115 or 230 volts $\pm 10 \%, 50$ to $1000 \mathrm{cps}, 2-1 / 2$ watts
Dimensions:
$6-17 / 32$ in. ( 16.6 cm ) high, $7-25 / 32$ in. ( 19.77 cm ) wide, $12-1 / 2 \mathrm{in} .(31.75 \mathrm{~cm}$ ) deep

## Weight:

Net $8 \mathrm{lb}(3.63 \mathrm{~kg})$ with cover and cables $11-1 / 2 \mathrm{lb}$
( 5.44 kg ) including battery; shipping approx. 13 lb
$(5.9 \mathrm{~kg})$

Accessories Furnished:
5 ft ( 1.5 m ) cable for (5) temperature-compensated thermistor mounts. $7-1 / 2 \mathrm{ft}(2.3 \mathrm{~m})$ power cable, NEMA plug.

Accessories Available:
431A-95A Rechargeable Battery Pack for field installation.

Models 478A and 486A Thermistor Mounts
(50) Model 8402A Power Meter Calibrator
(5i9) Model H01-8401A Leveler Amplifier
Options:

1. Rechargeable battery installed, provides up to 24 hours continuous operation,
2. Rear input connector wired in parallel with front panel input connector,
3. With 20 foot cable for $100 \Omega$ or $200 \Omega$ mount,
4. With 50 foot cable for $100 \Omega$ mount,
5. With 100 foot cable for $100 \Omega$ mount,
6. With 200 foot cable for $100 \Omega$ mount,
7. With 50 foot cable for $200 \Omega$ mount,
8. With 100 foot cable for $200 \Omega$ mount,
9. With 200 foot cable for $200 \Omega$ mount.

Table 1-2. Model 431B Thermistor Mounts

| Type |  | Frequency Range | Operating Resistance in ohms |
| :---: | :---: | :---: | :---: |
| Coaxial | Waveguide |  |  |
| (50) 478 A |  | 10 mc to 10 gc | 200 |
|  | (4p) S486A | 2.6 to 3.95 gc | 100 |
|  | (5ip) G486A | 3.95 to 5.85 gc | 100 |
|  | (5i) J486A | 5.3 to 8.2 gc | 100 |
|  | (5ip) H486A | 7.05 to 10.0 gc | 100 |
|  | (49) X486A | 8.2 to 12.4 gc | 100 |
|  | (4) M486A | 10.0 to 15.0 gc | 100 |
|  | (6) P486A | 12.4 to 18.0 gc | 100 |
|  | (50) K486A <br> (50) K486AC* | 18.0 to 26.5 | 200 |
|  | (5) R486A <br> (50) R486AC* | 26.5 to 40.0 | 200 |
| * With circular contact flange adapter |  |  |  |

1-5. The Model 431B has provisions for using the dc substitution method of measurement and for checking calibration accuracy of the power meter. The dc substitution method of measurement which requires other equipment provides greater power measurement accuracies than can be obtained by the power meter
alone. In addition a jack in series with the panel meter permits digital or chart recording of measurements, operation of alarm or control systems and use in a closed-loop leveling system.

## 1-6. ACCESSORIES.

1-7. Two accessories are supplied with the Model 431B Power Meter: a 7-1/2-foot, detachable power cable and a 5-foot cable that connects the thermistor mount to the Model 431B. Thermistor mounts are available (see table 1-2) but not supplied with the instrument. A rechargeable battery with installation kit is also available. A list of supplied and available accessories is given in table 1-1, Specifications.

## 1-8. INSTRUMENTS WITH OPTIONS.

1-9. The options available with the Model 431B Power Meter are given in table 1-1. The thermistor mount cable options require modification and recalibration of the Model 431B Power Meter. The recalibration procedures for the cables are given in section V, Maintenance. For further information as to the ordering of options etc., contact your local $\frac{10}{\infty}$ Engineering Representative.

## 1-10. INSTRUMENT IDENTIFICATION.

1-11. Hewlett-Packard uses a two-section eight-digit serial number ( $000-00000$ ). If the first three digits of the serial number on your instrument do not agree with those on the title page of this manual, change sheets supplied with the manual will define differences between your instrument and the Model 431B described in this manual.

## SECTION II

## INSTALLATION

## 2-1. INSPECTION.

2-2. This instrument was carefully inspected both mechanically and electrically, before shipment. It should be physically free of mars or scratches and in perfect electrical order upon receipt. To confirm this, the instrument should be inspected for physical damage in transit. Also check for supplied accessories, and test the electrical performance of the instrument using the procedure outlined in paragraph 5-71. If there is damage or deficiency, see the warranty on the inside rear cover of this manual.

## 2-3. INSTALLATION.

2-4. The $\stackrel{\text { 布 Model 431B is fully transistorized; there- }}{ }$ fore no special cooling is required. However, the instrument should not be operated where the ambient temperature exceeds $55^{\circ} \mathrm{C}\left(140^{\circ} \mathrm{F}\right)$.

## 2-5. RACK MOUNTING.

2-6. The Model 431B is a submodular unit that when used alone can be bench mounted only. However, when used in combination with other submodular units it can be bench and/or rack mounted. The (bombining case and adapter frame are designed specifically for this purpose.

2-7. COMBINING CASE. The combining case is a full-module unit which accepts varying combinations of submodular units. Being a full-module unit, it can be bench or rack mounted analogous to any full-module instrument. An illustration of the combining case is shown in figure 2-1. Instructions for installing the Model 431B in a combining case is given graphically in figure 2-2.

2-8. ADAPTER FRAME. The adapter frame is a rack frame that accepts any combination of submodular units. It can be rack mounted only. An illustration of the adapter frame is given in figure 2-3. Instructions are given below;
a. Place the adapter frame on edge of bench as shown in step (1), figure 2-4.
b. Stack the submodular units in the frame as shown in step (2), figure 2-4. Place the spacer clamps between instruments as shown in step (3), figure 2-4.
c. Place spacer clamps on the two end instruments (see step (4), figure 2-4) and push the combination into the frame.


Figure 2-1. The Combining Case


Figure 2-2. Steps to Place Instrument into Combining Case


Figure 2-3. Adapter Frame Instrument Combinations
d. Insert screws on either side of frame, and tighten until submodular instruments are tight in the frame.
e. The complete assembly is ready for rack mounting.

## 2-9. THREE-CONDUCTOR POWER CABLE.

2-10. To protect operating personnel, the National Electrical Manufacturers' Association (NEMA) recommends that the instrument panel and cabinet be grounded. All Hewlett-Packard instruments are equipped with a three-conductor power cable which, when plugged into an appropriate receptacle, grounds the instrument. The offset pin on the power cable three-prong connector is the ground wire.

2-11. To preserve the protection feature when operating the instrument from a two-contact outlet, use a three-prong to two-prong adapter and connect the green pigtail on the adapter to ground.

## 2-12. PRIMARY POWER REQUIREMENTS.

2-13. The Model 431B can be operated from an ac or dc primary power source. The ac source can be either 115 or 230 volts, 50 to 1000 cps . The dc source is a 24-volt rechargeable battery. The rechargeable battery is supplied with option 01 instruments only.

2-14. For operation from ac primary power, the instrument can be easily converted from 115- to 230volt operation. The LINE VOLTAGE switch, S1 a two-position slide switch located at the rear of the instrument, selects the mode of ac operation. The line voltage for which the instrument is set to operate appears on the slider of the switch. A 15/100-ampere, slow-blow fuse is used for both 115- and 230-volt operation.

## CAUTION

## DO NOT CHANGE THE SETTING OF THE LINE VOLTAGE SWITCH WHEN THE POWER METER IS OPERATING.

## 2-15. INITLAL BATTERY OPERATION CHECK.

2-16. The following applies to option 01 instruments or instruments that have field-installed batteries. When the battery is used as the Model 431B power source for the first time, perform the following steps:
a. Connect Model 431B to ac source. Set POWER switch to CHARGE and charge battery for a minimum of 16 hours or overnight. Note: the battery can be maintained in the charging state indefinitely without damaging the battery. It will assume its full capacity, 1.25 ampere hour, and no more.
b. Perform turn-on procedure given in figure 3-2 with POWER at AC. If the procedure checks out normally, proceed to step c.


Figure 2-4. Two Half Module in Rack Adapter
c. Repeat turn-on procedure given in figure 3-2 with POWER at BATTERY ON. If operation is not the same as that obtained with ac power applied, refer to section V paragraph 5-40, Battery and Charging Check.

## 2-17. REPACKAGING FOR SHIPMENT.

$2-18$. The Model 431B is shipped in a foam-pack and cardboard carton (see figure $2-5$ ). When repackaging the instrument for shipment, the original foam-pack and cardboard carton can be used if available. If not available, they can be purchased from Hewlett-Packard Co. (refer to section VI, misc). Use the following as a general guide for repackaging the instrument.
a. Place the instrument in the foam-pack as shown in figure 2-5.
b. Mark the packing box with "Fragile", "Delicate Instrument'', etc as appropriate.

## Note

If the instrument is to be shipped to HewlettPackard for service or repair, attach to the instrument a tag identifying the owner and indicating the service or repair to be accomplished, include the model number, and full serial number, of the instrument. In any correspondence, identify the instrument by model number, serial number and serial number prefix.


Figure 2-5. Repackaging for Shipment

# SECTION III <br> OPERATION 

## 3-1. INTRODUCTION.

3-2. The (50) Model 431B Power Meter measures rf power ranging from .01 to 10 milliwatts with power meter accuracy of $\pm 3 \%$. Since the zero carries over within $1 \%$, accuracies of at least $\pm 4 \%$ can be obtained on any range by a single zeroing on only the lowest range.

## 3-3. MECHANICAL ADJUSTMENT OF METER ZERO.

3-4. The procedure for performing the mechanical adjustment of the meter zero is given in section $V$, paragraph 5-54.

## 3-5. CONTROLS AND INDICATORS.

3-6. The front and rear panel controls and connectors are explained in figure 3-1. The explanations are keyed to corresponding controls and indicator on the drawing of the front and rear panels of the instrument provided with the figure.

## 3-7. OPERATING INSTRUCTION.

3-8. Figure 3-2, Turn-On and Nulling Procedure, and figure 3-3, DC Substitution Technique, give step-by-step instructions for operating the Model 431B. In figure 3-2, each step is numbered to correspond with numbers on the accompanying drawing of the power meter.

## 3-9. BATTERY OPERATION.

3-10. The following applies to power meters having a factory or a field-installed rechargeable nickel-cadmium battery. See figure 3-1, Turn-On and Nulling Procedure, for step-by-step instructions for operating the Model 431B from a battery.

## 3-11. BATTERY CHARGING TIMES.

3-12. The battery used in the Model 431B requires two hours of charge time for one hour of battery operation. When the battery is fully charged, the Model 431B can be continuously operated for 24 hours with 48 hours of charge time. However, it is recommended that battery operated instruments be operated for eight hour periods with a 16 hour recharge time. This makes the Model 431B available for portable use daily, yet maintains the battery at full charge.

## 3-13. BATTERY CHARGE CHECK.

3-14. Under normal conditions, a fully charged battery will start at approximately 27 volts and drop to about 22 volts after 24 hours of continuous use at room temperature.
a. Connect the Model 431B to ac primary power. Set POWER to AC and perform the turn-on and nulling
procedure given in figure 3-2. This will check for normal operation from ac primary power. If performance is normal proceed to step b.
b. Set POWER to BATTERY CHARGE: the AC CHARGE lamp will glow. Allow Model 431B to charge the battery for 48 hours. This will allow the battery to obtain a full charge.
c. After the recharge interval, set POWER to BATTERY ON. Since battery is now fully charged, you should be able to zero-set and null the meter (figure 3-2). If not the battery or battery charging circuit is at fault. Refer to Battery and Charging Checks paragraph 5-40.

## 3-15. MAJOR SOURCES OF ERROR, MICROWAVE POWER MEASUREMENTS.

3-16. In microwave power measurements, the following are the major sources of error: 1) mismatch error or tuner loss (when a tuner is used to tune out mismatch error), 2) bolometer mount efficiency, 3) substitution error, 4) instrument error and 5) error due to the unilateral properties of a thermistor. Thus five errors must be known if accurate power measurements are to be obtained. Expressed mathematically:

Total measurement error $=$
mismatch (or tuner) loss + calibration factor + instrument error + error due to the unilateral properties of a thermistor.
a. Mismatch Loss. Unless the mount and rf source are perfectly matched to the transmission system, a fraction of incident power is reflected and does not reach the thermistor. Since there generally is more than one source of mismatch in a microwave measurement system and the resulting error signals interact, loss cannot be calculated from the swr figure, it can only be expressed laying between two limits. Limits of mismatch loss generally are determined by means of a chart such as the Mismatch Loss Limits chart included in each of the thermistor mount Operating Notes. A tuner such as the (ara) Model 872A or 870 A can be used to minimize loss, although the tuner itself will introduce some loss.
b. Bolometer Mount Efficiency and Substitution Error. Not all the rf power applied to the mount is used to heat the rf thermistor. Some of it is absorbed by the other elements in the mount, such as the walls of the rf chamber, the heat sinks, the leads, etc. Substitution error results because rf power does not affect the thermistor to the same degree as dc power. Substitution error and mount efficiency are often combined for a simplicity of measurement into what is termed "calibration factor". Typically, the calibration factor of the Model X486A waveguide mount is $97 \%$ to $98 \%$.


1. POWER: The POWER switch sets up connections to the selected power sources or to the battery charging circuit. When the power switch is in the AC position, externally supplied 115 or 230 volts is applied to the instrument. If the instrument contains a battery, a trickle charge is applied to maintain the battery at full charge. With POWER at BATTERY ON, a 24 -vdc battery within the instrument supplies primary power to the instrument. With POWER at CHARGE, 115 - and 230 -volt power is used to charge the battery ( 16 to 24 hours is required to. obtain full battery charge). The instrument is inoperative in this position. Note: Batteries are installed at the factory for option 01 instruments only.
2. RANGE: The RANGE switch can be set for full scale power readings from .01 to 10 milliwatts in seven steps. It also includes a NULL position which, in conjunction with the adjacent null screwdriver adjust, insures that the metering bridge is reactively balanced.
3. THERMISTOR MOUNT: The THERMISTOR MOUNT connector is a female receptacle that accepts a specially-made cable which is supplied with the instrument. The cable connects the mount thermistors into their respective bridges within the power meter.

4. MOUNT RES: This two-position slide switch sets the power meter to accommodate thermistor mounts 100 - or 200 -ohm nominal resistance.
5. ZERO and VERNIER: The ZERO control coarsely sets the meter pointer near zero; the VERNIER control is a more exact adjustment which sets the meter pointer on zero.
6. DC CALIBRATION \& SUBSTITUTION. This terminal permits application of known direct current to the rf bridge. The power reading obtained with the accurately known de power applied is then compared with the reading obtained when rf power was applied. The dc substitution technique is used to both calibrate and increase the accuracy of 431B power measurement.
7. RECORDER: The RECORDER jack is a twowire telephone jack (one side grounded) for monitoring the current which operates the Model 431B meter.
8. LINE VOLTAGE: The LINE VOLTAGE switch S1, is a two-position slide switch that selects the mode of ac operation. The line voltage for which the instrument is set to operate appears on the slider of the switch. A 15/100 slow-blow fuse is used for both 115 and 230 volt operation.

Figure 3-1. Front and Rear Panel Controls and Indicators


1. Connect thermistor mount and cable to the THERMISTOR MOUNT. (50) thermistor mounts and their frequency ranges are given in table 1-2, Model 431B Thermistor Mounts.

## Note

When possible, the Model 431B should be zeroed and nulled with the power source to be measured connected to the thermistor mount. If this is not possible, and a coaxial thermistor mount is used, terminate the rf input into a 50 -ohm load. Power source should be off while zero and null-setting the Model 431B Power Meter.
2. Set MOUNT RES to match thermistor mount resistance ( 100 or 200 ohms).
3. Set RANGE to .01 MW .
4. Set POWER to AC; AC \& CHARGE lamp will glow. If instrument is battery-operated, rotate POWER to BATTERY ON.
5. Adjust ZERO control for 25 to $75 \%$ of full scale on meter.
6. Rotate RANGE to NULL and adjust null screwdriver adjust (adjacent to NULL on RANGE switch) for a minimum reading in NULL region.
7. Repeat steps 5 and 6 until NULL reading is obtained within NULL region on the meter.

## Note

If instrument is battery-operated and you are not able to zero the meter, or if meter pointer fluctuates rapidly, battery needs recharging. Refer to paragraph 3-11.
8. Set RANGE switch to the power range to be used and zero-set the meter with ZERO and VERNIER controls.

## Note

Zero-set accuracy of $1 \%$ can be obtained by zero setting the meter on the most sensitive range (. 01 MW ) only, and assuming the meter is properly zeroed on all less sensitive ranges. For maximum accuracy, zero set the meter on the range to be used.
9. Apply rf power at the thermistor mount and read power on Model 431B meter. Power is indicated on the meter directly in mw or dbm .

## Note

This instrument is accurate to within $\pm 3 \%$. Accuracy to $\pm 1 \%$, or better, is possible using the de substitution technique described in figure 3-3. See also paragraphs 3-15 and 3-17.


1. With power supply turned off, connect the Model 431B as shown above.
2. Set the Model 431B for normal operation on the appropriate range using the procedure given in figure 3-2.
3. Apply rf power at the thermistor mount and note and record the reading of the Model 431B meter. This is the reference for the substitution measurement.

## Note

A second digital voltmeter, in parallel with a 1000 -ohm ( $\pm 10 \%, 1$ watt) resistor, connected in series with the RECORDER output of the Model 431B will increase accuracy of reference duplication.
4. Turn off, or disconnect, the rf source.
5. Turn power supply on; adjust the output voltage of the power supply until the reference of step 3 is duplicated. A potentiometer arrangement may be substituted for the adjustable power supply. However, at least 10,000 ohms must remain in series with the supply.

## CAUTION

Never apply more than 20 ma dc to the DC CALIBRATION SUBSTITUTION terminals of the Model 431B.
6. Read the voltmeter with monitors the substitution current. The voltmeter reading can be interpreted as current in milliamperes because the voltage is measured across 1000 ohms. This current is $\mathrm{I}_{\mathrm{dc}}$.
7. Calculate power in mw from the expression

$$
\operatorname{Power}(\mathrm{MW})=\frac{\mathrm{I}_{\mathrm{dc}}^{2} \mathrm{R}_{\mathrm{d}}}{4 \times 10^{3}}
$$

where $R_{d}=$ operating resistance of the termistor ( 100 or 200 ohms)
and $I_{d c}=$ substitution current in milliamps (from step 6)
9. To minimize error due to drift in either the reference or substituted power level, steps 1 through 6 should be repeated.
c. Instrument Error. This is the inability of the power meter to accurately measure and interpret the information available at the thermistor element. In specifying the accuracy of a power meter, instrument error is the figure usually given. For the Model 431B, instrument error is $\pm 3 \%$ of full scale, $20^{\circ} \mathrm{C}$ to $35^{\circ} \mathrm{C}$. This error can be reduced by special techniques such as the de substitution method discussed in para. 3-17.
d. Error Due to the Unilateral Properties of a Thermistor. The thermistor used in conjunction with the Model 431A/B exhibits unilateral properties which, when the source of power is a dc current, causes a slightly different indication of power than is obtained by the calculation of $I^{2} R$. Thus the dc power required to produce a reading on the Model 431A/B Power Meter is not the same as the rf power required to produce the same reading on the Model 431A/BPower Meter. The maximum error produced from this source of error is $\pm 0.3 \mu$ watts, typical error is $\pm 0.1 \mu$ watt. Since the order of magnitude of this error is small ( $0.3 \mu \mathrm{watt}$ ) it need be minimized only on the two most sensitive ranges of the Model 431A/B Power Meter. Refer to the Model 8402A Power Meter Calibrator manual for procedure used to minimize this error.

## 3-17. POWER METER ACCURACY OF $1 \%$ OR GREATER USING THE DC SUBSTITUTION METHOD.

3-18. Highly accurate instruments are available for measuring direct current. Thus, where optimum accuracy is required, there is considerable advantage in using a technique where the rf measurement is used only as a reference and the determination of rf power is based on precise de measurements. In general the technique involves:
a. Applying rf power to the Model 431B in the usual manner, and noting the resulting meter indication for use as a reference.
b. Removing the rf power and applying sufficient dc at the DC CALIBRATION \& SUBSTITUTION terminals to exactly duplicate the meter indication produced by the rf power.
c. Use the value of dc which duplicated the reference in calculating rf power.

3-19. Although the dc substitution technique is the most accurate method of measuring rf power, there are sources of error that must be considered. The accuracy of the dc substitution technique depends largely upon:
a. how precisely the reference is duplicated,
b. how accurately the value of the substituted dc is known,
c. the actual operating resistance of the thermistor, and
d. the actual ratio of current division in the rf bridge.

3-20. With precision components in the substitution setup and careful procedure, error produced by the Model 431B Power Meter can be reduced to $1 \%$ or less. This is assuming nominal thermistor mount resistance ( 100 or 200 ohms) and that half the applied de flows through the rf thermistor. The dc substitution technique using the Model 431B is shown in figure 3-3.

## 3-21. EQUIPMENT USEDFOR DC SUBSTITUTION.

3-22. The (bip) Model 8402A Power Meter Calibrator was specifically designed to be used for calibration and de substitution measurements of rf power. In addition, the instrument will accurately measure the operating resistance of the thermistor mount being used. Use the procedures given in the manual provided with the (70) Model 8402A Power Meter Calibrator to perform the dc substitution measurements.

3-23. Although the most convenient and accurate means of applying the dc substitution technique is by using (50) Model 8402A Power Meter Calibrator, it is also possible to accurately measure power using the dc substitution technique with the arrangement shown in figure 3-3. The digital voltmeter is used to monitor the substitution current. The power supply output and voltmeter input are ungrounded to eliminate ground currents.

## 3-24. ADDITIONAL APPLICATIONS.

$3-25$. At the RECORDER output, the Model 431B furnishes a current ( 0 to 1 ma de ) which is proportional to the power measured. This feature makes possible a measurement system with more capability than simply the indication of power on a meter. Some of the more sophisticated measurement systems are shown in block diagram form in figures 3-4 through 3-8.

3-26. PERMANENT RECORD. Use of a recorder in the measurement system is indicated in figure 3-4. Resistance across the Model 431B RECORDER output must be 1000 ohms. Any type of recorder may be used with the Model 431B; if input resistance exceeds 1000 ohms, use a shunt across the recorder input.


Figure 3-4. Permanent Record


Figure 3-5. Increased Resolution

3-27. INCREASED RESOLUTION. Digital readout of power to three decimal places can be obtained with the arrangement shown in figure $3-5$. The value of R1 is 316.2 ohms $\pm .1 \%$ and $R_{t}$ is 1000 ohms $\pm .1 \%$. Correct placement of the decimal in the readout is determined by the setting of the power meter RANGE switch. On the divider-switch arrangement at the voltmeter input may be replaced by a single 1000 -ohm $.1 \%$ resistor. With this arrangement, on the $.01, .1$, and 10 MW ranges, power is read in the same way as when the arrangement shown in figure $3-5$ is used, decimal placement being determined by the setting of RANGE. On the $.03, .3$, and 3 MW ranges, however to obtain the power readings the voltmeter indication must be multiplied by the factor given in table 3-1.

Table 3-1. Voltmeter Readout to Power Multipliers

| Range | Multiplier |
| :--- | :--- |
| .03 MW | 0.0316 |
| .3 | 0.316 |
| 3 | 3.16 |

3-28. LEVELER. Figure $3-6$ is a block diagram of a closed-loop control circuit for maintaining output power at a constant level. It is recommended for use in leveling the output of various types of 有 microwave equipment such as bwo sweep oscillators, twt microwave amplifiers, and rf generators. In addition to the

Model 431B and its thermistor mount, such a leveling system requires the (6p) H01-8401A Leveler Amplifier and a directional coupler with good directivity such as one of the 752 series of waveguide couplers or 760 series of coaxial couplers. The output of the power source is sampled by the coupler and applied to the Model 431B. A dc signal, proportional to the power sample, is fed (from the Model 431B RECORDER jack) to the Leveler Amplifier. In the H01-8401A the signal from the Model 431B is compared to an internal reference voltage, and the difference is amplified and fed back as a control voltage to hold output power constant.

## 3-29. MONITOR CONTROL SYSTEMS. By adding a

 dc amplifier and relay circuit to the rf monitoring arm of a system, the de signal provided by the Model 431B can be used to actuate alarm or control circuits. Arrangement of equipment to provide an alarm or control system is shown in block diagram form in figure 3-7.3-30. DETERMINING INSERTION LOSS OR GAIN AS A FUNCTION OF FREQUENCY. Arrangement of a system to obtain information on insertion loss or gain as a function of frequency is indicated in figure 3-8. Initially, the device under test is not connected into the system; connect the thermistor mount directly to the sweep oscillator. Set the sweep oscillator for the band of interest, and record variations in amplitude as frequency is swept; this curve is the reference. Next, insert the device under test between the sweep oscillator and the thermistor mount, and again record frequency response. The difference between the second reading and the reference, at any one frequency, is the insertion loss or gain of the device at that frequency.


Figure 3-6. Leveler Setup


Figure 3-7. Monitor Control Systems


Figure 3-8. Determining Insertion Loss or Gain


Figure 4-1. Block Diagram

# SECTION IV THEORY OF OPERATION 

## 4-1. OVERALL DESCRIPTION.

4-2. Figure 4-1 is a block diagram which shows the Model 431B Power Meter and its associated thermistor mount. The thermistor mount contains two thermistor elements ( $\mathrm{R}_{\mathrm{d}}$ and $\mathrm{R}_{\mathrm{c}}$ ). Thermistor element $\mathrm{R}_{\mathrm{d}}$ absorbs the rf power applied to the mount; thermistor element $\mathrm{R}_{\mathrm{c}}$ converts the applied rf power to a meter indication and provides compensation for ambient temperature changes at the thermistor mount.

4-3. The power meter circuitry incorporates two bridges which are made self-balancing by means of separate feedback loops. Regenerative (positive) feedback is used in the detection loop; degenerative feedback in the metering loop. One thermistor element is used in one arm of each of the self-balancing bridges. In the detection loop, the 10 kc oscillator-amplifier supplies enough 10 kc power ( $\mathrm{I}_{10 \mathrm{kc}}$ ) to bias thermistor element $\mathrm{R}_{\mathrm{d}}$ to the operating resistance which balances the rf bridge. The same amount of 10 kc power is also supplied to thermistor element $R_{c}$ by the series-connected primaries of transformers T101 and T102.

4-4. When rf power is applied to thermistor element $R_{d}$, an amount of 10 kc power equal to the rf power is removed from thermistor element $R_{d}$ by the selfbalancing action of the rf bridge. Since the primaries of T101 and T102 are series-connected, the same amount of 10 kc power is also removed from thermistor element $R_{c}$, thus, the action which balances the rf bridge unbalances the metering bridge. The metering bridge loop automatically re-balances by substituting dc power for 10 kc power. Since the 10 kc power equaled the applied rf power, the substituted dc power is also equal to the applied rf power. Instead of metering the feedback current directly, which would require the use of a nonlinear meter scale, an analog current is derived which is proportional to the square of the feedback. Since power is a square-law function of current, the analog current thus derived is proportional to rf power, making possible the use of a linear scale on the meter.

4-5. There is little drift of the power meter zero point when ambient temperature at the thermistor mount changes. If, for example, ambient temperature at the mount increases, a decrease in electrical power to the thermistors is required to hold their operating resistances constant. The decrease, for both thermistors, is made automatically by the detection loop (figure 4-1) which reduces 10 kc power. The amount of dc power in the metering loop remains unchanged however, and since this dc power controls the meter action, the ambient temperature changes does not affect the meter indication. The compensation capability depends upon the match of thermistor temperature characteristics. When thermistor mounts are built, the thermistors are selected to insure optimum match of thermal characteristics.

## 4-6. CIRCUIT DESCRIPTION.

## 4-7. RF BRIDGE CIRCUIT.

4-8. A simplified schematic diagram of the rf bridge circuit is shown in figure $4-2$. The rf bridge circuit consists of the rf bridge and $10-\mathrm{kc}$ oscillator-amplifier. The rf bridge includes thermistor $R_{d}$, the secondary winding of T101, resistors R102 and R103, the MOUNT RES switch, $S 2$, and capacitance represented by $C_{a}$ and $\mathrm{C}_{\mathrm{b}}$. The rf bridge and 10 kc oscillator-amplifier are connected in a closed loop (the detection loop) which provides regenerative feedback for the oscillatoramplifier. This feedback causes the 10 kc oscillatoramplifier to oscillate.

4-9. When the power meter is off, thermistor $R_{d}$ is at ambient temperature and its resistance is about 1500 ohms; the rf bridge is unbalanced. When the power meter is turned on this unbalance of the rf bridge causes a large error signal to be applied to the 10 kc oscillator-amplifier. Consequently maximum 10 kc bias voltage is applied to the rf bridge. As this 10 kc voltage biases $R_{d}$ to its operating resistance (100 or 200 ohms) the rf bridge approaches a state of balance and regenerative feedback diminishes until there is just sufficient 10 kc bias power to hold $\mathrm{R}_{\mathrm{d}}$ at operating resistance. This condition is equilibrium for the detection loop.

4-10. With application of rf power, thermistor $\mathrm{R}_{\mathrm{d}}$ 's resistance decreases causing the regenerative signal from the rf bridge to decrease. Accordingly, 10 kc power diminishes, the thermistor returns to operating resistance and the detection loop regains equilibrium.

4-11. The MOUNT RES switch, S101, changes the resistance arm of the rf bridge so that the bridge will function with either a 100 or 200 ohm thermistor mount.


Figure 4-2. RF Circuit

## 4-12. METERING BRIDGE CIRCUIT.

4-13. A simplified schematic diagram of the metering bridge circuit is shown in figure 4-3. Operation of the metering bridge circuit is similar to the rf bridge circuit. It uses the same principle of self-balancing through a closed loop (metering loop). The major difference is that dc rather than $10-\mathrm{kc}$ power is used to rebalance the loop. The resistive balance point is adjusted by the ZERO and VERNIER controls which constitute one arm of the bridge. The MOUNT RES switch (not shown in figure 4-3) which is mechanically linked to both the rf bridge and metering bridge, changes metering bridge reference resistance from 100 to 200 ohms. When the MOUNT RES switch is in the 200 -ohm position some of the feedback current is shunted to ground through R101. This maintains the $I^{2} \mathrm{R}$ function constant when mount resistance is changed from 100 or 200 ohms. The switch also adds the necessary reactance for each position.
4-14. The same 10 kc power change produced in the rf bridge by rf power also affects the metering bridge through the series connection of T101 and T102 primaries. Although this change of $10-\mathrm{kc}$ power has equal effect on both the rf and metering bridges, it is initiated by the rf bridge circuit alone. The metering bridge cannot control $10-\mathrm{kc}$ bias power, but the $10-\mathrm{kc}$ bias power does affect the metering circuit. Once a change in the $10-\mathrm{kc}$ bias power has affected (unbalanced) the metering bridge, a separate, closed dc feedback loop (metering loop) re-establishes equilibrium in the metering circuit.
4-15. Variations in $10-\mathrm{kc}$ bias level, initiated in the rf bridge circuit, cause proportional unbalance of the metering bridge, and there is a change in the $10-\mathrm{kc}$ error signal ( $\mathrm{S}_{10} \mathrm{kc}$ ) applied to the $10-\mathrm{kc}$ tuned amplifiers in the metering loop. These error signal variations are amplified by three $10-\mathrm{kc}$ amplifiers, and rectified by the synchronous detector. From the synchronous detector the dc equivalent ( $I_{d c}$ ) of the $10-\mathrm{kc}$ signal is returned to the metering bridge, and is monitored by the metering circuit to be indicated by the meter. This dc feedback to the metering bridge acts to return bridge to its normal, near-balance condition.


Figure 4-3. Metering Bridge Circuit


Figure 4-4. Nulling Circuit
4-16. The reactive components of the metering bridge are balanced with variable capacitor C103 and inductor L102. Null adjust, C103, is an operational adjustment and L102 is a maintenance adjustment. Null adjust C103, is adjusted with the RANGE switch in the NULL position. A simplified schematic diagram of the NULL circuit is shown in figure $4-4$. The 10 kc signal is taken at the synchronous detector, rectified by CR105, and read on the meter. The rectified signal contains both reactive and resistive voltage components of the bridge unbalance.

## 4-17. SYNCHRONOUS DETECTOR.

$4-18$. The synchronous detector converts the $10-\mathrm{kc}$ error signal from the metering bridge to a varying dc signal. A simplified schematic of the synchronous detector is shown in figure 4-5. The detector is a bridge rectifier which has a rectifier in series with a linearizing resistance in each of its arms. Two $10-\mathrm{kc}$ voltages, designated E3 and E4 in figure 4-5, are applied to the bridge; 1) voltage E3, induced in the secondary of transformer T103, is proportional to the metering-bridge error signal and is incoming from $10-\mathrm{kc}$ tuned amplifier Q103; 2) voltage E4, induced in the secondary of T104, is proportional to a voltage supplied by the $10-\mathrm{kc}$ oscillator-amplifier. Voltage E4 is much larger than voltage E3 and switches appropriate diodes in and out of the circuit to rectify voltage E3. Section A of figure 4-5 shows the current path through diodes CR102 and CR104 for a positive-going signal; section B shows the current path through diodes CR101 and CR103 for a negative-going signal. The rectified output is taken at the center taps of transformers T103 and T104.

4-19. Operation of the circuit is as follows: When the left side of T104 is positive with respect to the right side (see figure 4-5A), diodes CR102 and CR104 conduct while diodes CR101 and CR103 are biased off. With the polarities reversed (see figure $4-5 B$ ), the


Figure 4-5. Synchronous Detector
diodes CR102 and CR104 are biased off. The resultant output is a pulsating de signal equivalent to the applied $10-\mathrm{kc}$ error signal. This pulsating de signal is filtered and applied to differential amplifier Q104/Q105.

4-20. Proper synchronous detector output requires an in phase relationship between E3 and E4 and for amplitude of E 4 to be larger than that of E 3 .

4-21. DIFFERENTIAL AMPLIFIER Q104/Q105.
4-22. A simplified schematic diagram of the amplifier is shown in figure 4-6. The pulsating dc from the synchronous detector is filtered by C117, C118, C119,


Figure 4-6. Differential Amplifier


Figure 4-7. Feedback Current Generator
and R140, amplified by Q104 and fed to both the feedback current-squared generator, Q106 (figure 4-7) and feedback current generator Q107. Temperature compensation and low emitter circuit resistance for Q107 are provided by Q105. Diode CR106 protects Q106 and Q107 from excessive reverse bias when Q104 is cut off.

## 4-23. FEEDBACK CURRENT GENERATOR Q107.

4-24. A simplified schematic diagram of the feedback current amplifier is shown in figure 4-7. The de signal from the differential amplifier is applied to feedback current generator Q107. Q107 has two functions: 1) it


Figure 4-8. Meter Circuit
completes the metering loop to the metering bridge, and 2) it operates in conjunction with the first $10-\mathrm{kc}$ amplifier, Q101, and the RANGE switch to change metering loop gain so that the meter will read full scale for each power range. Diode CR107 provides additional temperature compensation for Q107.

## 4-25. METER CIRCUIT.

4-26. The meter circuit is shown in figure 4-8. It includes feedback current-squared generator Q106, a squaring circuit, the meter, and RECORDER jack, J102. The purpose of the meter circuit is to convert a linear voltage function, proportional to applied power, to a squared function so that power may be indicated on a linear meter scale. The linear voltage function is applied to the base of Q106 and is converted to a square law function by the squaring circuit in series with Q106 emitter.
4-27. SQUARING CIRCUIT. The squaring circuit includes diodes CR109-113, and resistors R167-177. Temperature compensation for the squaring circuit is provided by CR108.

4-28. The design of the squaring circuit is such that individual diodes conduct at discrete values of emitter voltage so that emitter conductance approximates a square law function. Thus the collector current of Q106 is made to approximate a square law function, and the meter indicates power on a linear scale.

4-29. RECORDER OUTPUT. The current which drives the meter can be monitored at the RECORDER output, a telephone-type two-wire jack. A RESISTOR OF 1000 OHMS MUST REMAIN IN SERIES WITH THE METER FOR ALL APPLICATIONS USING THE METER-DRIVING CURRENT.

4-30. ZEROING. Perfect balance of the metering bridge would mean that no 10 kc error signal would be applied to the 10 kc amplifiers, there would be no dc feedback from Q107, and the metering loop would be open. With an open metering loop, zero reference could not be accurately established. In the Model


Figure 4-9. DC Calibration and Substitution
431B this occurrence is prevented by insuring a closed metering loop even when the ZERO control causes the meter pointer to deflect downscale from zero. By the combined actions of R141 and R179, the zero setting of the meter pointer does not coincide with absolute balance of the metering bridge. A slight unbalance of the bridge is maintained by R141, while R179 provides a counter-action in the feedback current-squared generator, Q106, so that the meter can indicate zero even though the metering bridge is not perfectly balanced. Resistor R179 also sets the full scale accuracy of the meter.

## 4-31. DC CALIBRATION AND SUBSTITUTION.

4-32. A simplified schematic diagram of the dc calibration and substitution circuit is shown in figure 4-9. Highly accurate rf power measurements can be made using the dc substitution technique given in figure 3-3. In the dc substitution method dc is used to duplicate the rf power reading. An accurate, known current ( $\mathrm{I}_{\mathrm{dc}}$ ) is supplied externally at the DC CALIBRATION and SUBSTITUTION terminals. Calculation of the substituted dc power gives an accurate measure of the rf power. Effectively, dc power is substituted for rf power.

## 4-33. REGULATED POWER SUPPLY.

4-34. A simplified schematic diagram of the power supply is shown in figure 4-10. The power supply operates from either a 115 or 230 volt, 50 to 1000 cps ac source or from an optional 24 volt, 30 ma rechargeable battery. Three voltages and two current outputs are provided by the power supply. Regulated voltages of -18 and -25 vdc and unregulated +1.5 vdc operate the power meter circuits. The current outputs are used for maintaining battery charge (trickle charge) for recharging the battery.

4-35. The -18 vdc is regulated by a conventional series regulator, Q1 through Q5. The -25 vdc is developed across CR9, a 6.8 volt zener diode referenced at -18 vdc . The unregulated +1.5 vdc is taken
across the series diodes, CR5 and CR6. The -18 vdc supply is adjusted by R13.

4-36. POWER SWITCH.
4-37. A simplified schematic diagram of the power switching arrangement is shown in figure 4-11. The power switch, S2, has four positions: OFF, AC, BATTERY ON, and BATTERY CHARGE. In the AC position, the instrument operates from the conventional line voltage: if a battery has been installed in the instrument, a trickle charge is supplied to the battery. In the BATTERY ON position, instrument operation is entirely dependent on the battery. In the CHARGE position, supply A is connected to the battery for recharging: the Model 431B cannot be operated during this time. Approximately 37 ma dc is applied to the battery during charge time.


Figure 4-10. Regulated Power Supply


Figure 4-11. Power Switch Arrangement


Figure 5-1. Cover Removal

# SECTION V <br> MAINTENANCE 

## 5-1. INTRODUCTION.

5-2. This section includes instructions and information for the maintenance, troubleshooting and repair of the Model 431B Power Meter.

5-3. The testing and repair of 㐌 Model 486A and 478A thermistor mounts are not discussed in this manual. Complex procedures and special equipment are needed for these operations. Therefore, if the cause of trouble is proved to a thermistor mount, an (4p) Engineering Representative should be contacted or mount should be returned to factory (do not attempt to repair the thermistor mount).

## 5-4. COVER REMOVAL AND REPLACEMENT.

5-5. Refer to figure 5-1 when removing instrument covers. Removal of the top cover exposes the circuit areas shown in figure 5-2. Routine checks and adjustments can be performed without the removal of other covers. However, operations such as soldering on
the circuit board and removal of the meter, RANGE POWER, or MOUNT RES switch would require the removal of the bottom cover and one, or both, of the side covers.

5-6. TOP COVER REMOVAL.
a. At the rear of the instrument, remove the two screws which retain the cover.
b. Grasp the cover from the rear, slide in back $1 / 2$ inch, then tilt forward edge of the cover upward and lift the cover from the instrument.

## 5-7. TOP COVER REPLACEMENT.

a. Rest the cover flat on the cast guides projecting inward near the top of each side frame (see (1), figure 5-1).
b. Slide the cover forward allowing its forward edge to enter the groove in the front panel.
c. Replace the two cover retaining screws.

Table 5-1. Test Equipment

| Instrument Type | Use | Critical Specifications |  | Instrument Recommended |
| :---: | :---: | :---: | :---: | :---: |
| DC voltmeter | DC voltage measurement Calibration accuracy check | Range: 0.5 to 50 volts dc Accuracy: $\pm 0.2 \%$ <br> Resolution: three digit |  | (4) 405BR/CR |
| Ohmmeter | Continuity \& resistance checks | Range: 1 ohm to 10 megohms Accuracy: 5\% of full scale |  | (b) 410B <br> (90) 412A |
| Precision milliammeter or Power Meter Calibrator | Calibration accuracy check | Milliammeter | Accuracy: $0.1 \%$ of full scale <br> Range: 0 to 30 ma | Sensitive Research Instrument Corp Model B, Bamilek |
|  |  | Calibrator | Current accuracy: $0.1 \%$ <br> Resistance accuracy: $0.2 \%$ | (50) 8402A Power Meter Calibrator |
| Milliammeter | Battery circuit check | Range: 3 to 60 ma Accuracy: 5\% |  | $\begin{aligned} & \text { (ap 412A } \\ & \text { (5p) 428A/B } \end{aligned}$ |
| Oscilloscope or AC voltmeter | Power supply ripple check <br> 10 kc oscillatoramplifier check 10 kc amplifier check 10 kc amplifier null adjust | Oscilloscope | Bandwidth: 100 kc <br> Accuracy: 5\% <br> Input impedance: <br> 1 megohm <br> Sensitivity: $1 \mathrm{mw} / \mathrm{cm}$ | $\begin{aligned} & \text { (7p) } 130 \mathrm{~B} / \mathrm{C} \\ & \text { (40) } 120 \mathrm{~B} \\ & \text { (40) } 122 \mathrm{~A} \end{aligned}$ |
|  |  | AC voltmeter | Accuracy: 5\% <br> Input impedance: <br> 1 megohm <br> Range: . 01 to 100 mv | $\begin{aligned} & \text { (90) } 400 \mathrm{D} / \mathrm{H} / \mathrm{L} \\ & \text { (40) } 403 \mathrm{~A} / \mathrm{B} \end{aligned}$ |

Table 5-1. Test Equipment (Cont'd)

| Instrument Type | Use | Critical Specifications | Instrument Recommended |
| :---: | :---: | :---: | :---: |
| DC Source or Power Meter Calibrator | Calibration accuracy check | Range: 0 to 220 vdc or Current Output: 0 to 20 ma | (50) 711A, 712B Power Supplies 8402A Power Meter Calibrator |
| Thermistor Mount | Completion of test circuit | See table 1-2 for list of suitable mounts |  |
| Transformer to vary line voltage | Power supply regulation check |  | General Radio W5MT3A |
| Frequency counter | 10 kc oscillator amplifier check 10 kc oscillator-amplifier frequency adjust | 5 place readout Min. input sensitivity: 4 v rms Max. frequency: greater than 10 kc Accuracy: better than $0.1 \%$ | (59) 521 C or E <br> (420) 5212A <br> (40) 5512A |
| Variable Transformer | Power supply adjustment | Range: 103 to 127 vac @ 7-1/2 amp 206 to 254 vac @ 4 amp <br> Voltmeter range: 100 to 127 vac 200 to 254 vac <br> Voltmeter accuracy: $\pm 1$ volt | General Radio type W10MT3A |
| Soldering Iron \& Tips | Repair | Wattage rating: 50 watts Min tip temp: $800^{\circ} \mathrm{F}$ Tip size O.D.: $1 / 16^{\prime \prime}$ to $3 / 32$ | Ungar \#776 soldering iron handle Ungar \# PL333 tiplet Ungar \#854 Cup tip |
| Resistor | Charging checks | Value: $780 \Omega$ <br> Accuracy: $\pm 1 \%$ <br> Wattage: 3 watts | Dale Type RS-2 |
| Resistor | Charging checks | Value: $7500 \Omega$ <br> Accuracy: $\pm 1 \%$ <br> Wattage: 2 watts | Electra MF2, T-0 |
| Decade Resistance Divider | Zero and vernier control adjustment Full scale accuracy adj | Range: $50 \Omega$ to $50 \mathrm{~K} \Omega$ <br> Multiple: $10 \Omega$ <br> Accuracy: 1\% per decade | GR1432P Decade Resistance Box |
| Precision Resistor | Zero and vernier control adjustment | Value: $1000 \Omega$ <br> Accuracy: $\pm 0.1 \%$ <br> Wattage: 0.25 watts | Ultronex Type 205A |
| Decade Capacitors | Oscillator frequency adjustment Coarse null adjustment | Range: 10 to 1000 pf Capacitance per step: . $0001 \mu \mathrm{fd}$ Accuracy: . $1 \%$ per decade | General Radio Type 1419-B |

## 5-8. BOTTOM COVER REMOVAL.

a. Set the tilt stand as shown in figure 5-1.
b. Remove the two retaining screws at the rear of the cover.
c. Slide the cover rearward far enough to free its forward edge from the front foot assembly.
d. Tilt the forward edge of the cover upward and lift the cover from the instrument.

## 5-9. BOTTOM COVER REPLACEMENT.

a. Set the tilt stand as shown in figure 5-1.
b. Rest the bottom cover flat on the cast guides projecting inward near the bottom of each side frame (see (2), figure 5-1).
c. Slide the cover forward on the guides so that the formed portion at the rear of the cover slides over the two short projections at the rear corner of each side frame (see (3), figure 5-1).
d. Replace the two retaining screws and the rear foot assembly.

## 5-10. SIDE COVER REMOVAL.

$5-11$. The side covers cannot be removed until the top and bottom covers are off (see paragraphs 5-6 and 5-8). Each side cover is held in place by four screws retained by nuts which are not fastened to the side frames.

## Note

Replace side covers before replacing either the top or the bottom cover.

## 5-12. TEST EQUIPMENT.

5-13. Any instrument which satisfies the specifications of table 5-1 can be used for the test described in this maintenance section.

## 5-14. TROUBLESHOOTING.

5-15. The first step in troubleshooting the Model 431B Power Meter should be isolation of trouble to the thermistor mount and thermistor mount cable or to the power meter itself. The thermistor match check in the maintenance section of the ( 6 Operating Note pertaining to the thermistor mount in use will indicate a defective thermistor or thermistors. A simple ohmmeter continuity check and inspection of the thermistor mount cable and its connectors can be used to prove the cable.

5-16. Table 5-2, Troubleshooting, and the following detailed tests are given to aid in correcting trouble within the Model 431B. To make localizing of trouble easier, the 431B circuitry is divided into five sections; the power supply, the 10 kc oscillator-amplifier (including the rf bridge), the 10 kc amplifier (including the metering bridge), the dc metering and feedback amplifiers, and the squaring circuit. Tests are given for each of these sections.

## 5-17. THE POWER SUPPLY.

$5-18$. The de test point voltages shown on the power supply schematic diagram, with two exceptions, apply to instruments operated from either ac or battery primary power. Voltage limits shown at C1 and C2 apply only to instruments operated from ac primary power. Refer to figure 5-2, Top View, for component location.
a. Connect Model 431B to a variable line transformer and set transformer for 115 vac (or 230 vac ).
b. Connect a dc voltmeter (see table 5-1 for voltmeter requirements) between the negative terminal of C6 and Model 431B ground. The voltage here should be -18 vdc ; adjust with potentiometer R13.
c. With the voltmeter connected as above, test the regulation of the power supply (for instruments

Table 5-2. Troubleshooting

| Trouble Indication | Possible Cause |
| :---: | :---: |
| Null impossible | Thermistor mount Thermistor mount cable MOUNT RES switch T102 |
| Meter does not indicate, does not zero but does null | Q106 |
| Meter pointer drifts during readings | Thermistor mount Q106, Q107 <br> Thermistor mount in unstable thermal environment <br> RF source unstable <br> DC calibration/substitution source unstable <br> Oscillator-amplifier <br> 10 kc amplifier <br> Interference from external 10 kc signal |
| Rotation of the ZERO or VERNIER control results in erratic movement of the meter pointer on the . 01 MW range | ZERO or VERNIER potentiometer |
| Movement of the thermistor mount cable causes abrupt flicker of the meter pointer on the . 01 MW range | Thermistor mount Thermistor mount cable |
| Meter pointer stays down scale | T102 <br> Thermistor mount Thermistor mount cable Power supply Meter RECORDER jack Q106 C102, C101 10 kc amplifier |

Table 5-2. Troubleshooting (Cont'd)

| Trouble Indication | Possible Cause |
| :--- | :--- |
| Meter pointer stays up scale | T102 |
|  | Oscillator failure |
|  | Thermistor mount cable |
|  | Large unbalance in the metering bridge |
|  | C105 |
|  | C104 |
|  | 10 kc amplifier failure |
| Calibration inaccurate, all power ranges | Thermistor mount in strong rf field |
|  | Interference from stray 10 kc signal |
|  | Thermistor mount |
|  | Meter not mechanically zero-set |
|  | Meter |
|  | MOUNT RES switch |
|  | Power supply |
|  | Battery |
|  | 10 kc amplifier |
|  | Collector resistor R101 |
|  | Q107, Q106 |
|  | Q102 |
| Calibration inaccuracy, NOT all power ranges | Resistors emitter Q107 |
|  | Q106 |
|  | 10 kc amplifier |
| Zero setting does not carry over from range to | Q106 |
| range within specification | R141 |
|  | Q104 |

operated from ac primary power) by varying the line voltage $\pm 10 \%$ about the nominal 115 or 230 vac. There should be no perceptible variation of the -18 vdc.
d. If -18 volts cannot be obtained by adjustment of R13, or if regulation is not satisfactory, proceed with the following test to determine the causes:
(1) Use a dc voltmeter (see table 5-1) to check the ac voltage limits at the points listed in table 5-3. See figure 5-2, top view, for component location. All voltages are measured with reference to the Model 431B ground.
(2) Check ripple voltages (ac operation), using an ac voltmeter or oscilloscope, at the points listed in table 5-4. Table 5-1 gives requirements for the voltmeter or oscilloscope.

5-19. If the power meter does not function normally (e.g., pointer driven to its limits, no power indication) and power supply regulation is unsatisfactory, another circuit area, such at the 10 kc oscillator-amplifier or 10 kc amplifier, could be the cause.
$5-20$. A -18 vdc supply which is set high or low causes calibration inaccuracy of the Model 431B.

## 5-21. 10-KC OSCILLATOR-AMPLIFIER CHECK.

5-22. Tests of the oscillator-amplifier should be made according to the step sequence in which they appear below. A dc voltmeter, an ac voltmeter or oscilloscope and a frequency counter are needed for the tests (see table 5-1 for test instrument specifications). Figure 5-2, Top View, shows component location.

5-23. STEP 1.
a. Connect the oscilloscope between the positive lead of C125 and ground, check the 10 kc oscillatoramplifier output amplitude and waveform. Output amplitude, with a 200 ohm thermistor mount connected to the Model 431B, should be 15 vac $\pm 20 \%$ peak-to-peak. If a 100 -ohm mount is used, the amplitude should be 8 vac $\pm 20 \%$ peak-to-peak. The waveform must be sinusoidal with only slight crossover distortion (caused by Q110 and Q111).
b. Check the frequency of the oscillator-amplifier. If a Model 478A thermistor mount is used, terminate the rf input to the mount in 50 ohms. A Model 486A thermistor mount does not require termination. Connect the frequency counter between the positive lead of C125 and ground. With Model 478A thermistor mount connected to the Model 431B, the oscillatoramplifier frequency should be $9750-10,000 \mathrm{cps}$. With a Model 486A thermistor mount connected, the frequency should be $10 \mathrm{kc} \pm 50 \mathrm{cps}$.

## 5-24. STEP 2.

a. Connect the oscilloscope between the base of Q108 and ground; observe the amplitude of the feedback signal to the oscillator-amplifier. It must be less than 12 mv peak-to-peak: if not, 10 kc oscillatoramplifier gain is incorrect. The cause could be Q108, Q109, C124, L101, L105 or T101. If T101 is the cause of trouble use a special soldering tip to remove it from etched circuit board (see table 5-1).

Table 5-3. Power Supply DC Voltage Checks

| Test Point | DC Voltage Limits | Voltage Out of Limits, Check |
| :--- | :--- | :--- |
| Minus end of C1 | -38 to -43 | ac line voltage, CR1, CR4, C1 |
| Minus end of C2 | -24 to -27 | ac line voltage, CR2, CR3, C2, battery |
| Anode of CR8 | -10.7 to -12.3 | CR8 |
| Anode of CR7 | -6.0 to -7.5 | CR7, Q3 |
| Minus end of C6 | -18 | R13, Q5, Q2 |
| Base of Q1 | -18.3 to -18.6 | Q1, Q3, Q2, CR7 |
| Anode of CR9 | -24.0 to -25.6 | CR9, POWER switch |
| Plus end of C1 | +1.4 to +1.5 | CR5, CR6 |

Table 5-4. Power Supply Ripple Checks

| Test Point | AC Voltage Limits |  | Voltage Out of Limits, Check |
| :--- | :---: | :---: | :---: |
|  | R.M.S. | Peak-to-Peak |  |
| Minus end of C1 | 1.8 v max. | 5 v max. | CR1, CR4, C1 |
| Minus end of C2 | $1.1 \mathrm{v} \max$. | $3 \mathrm{v} \max$. | CR2, CR3, C2, C6, Q13 |
| Minus end of C6 | 10.6 mv max. | $30 \mathrm{mv} \max$. | Q1 to Q5, CR7, CR15, C2, C6 |

Table 5-5. 10 KC Oscillator-Amplifier DC Voltage Checks

| Test Point | DC Voltage Limits | Voltage Out of Limits, Check |
| :--- | :---: | :---: |
| Collector of Q110 | -18 | Power Supply |
| Emitter of Q109 | -10.0 to -14.0 | Q108, Q109, C122, C121 |
| Minus end of C121 | -5.0 to -6.5 | C121, Q108, R153 |

Table 5-6. 10 KC Amplifier DC Voltage Checks

| Test Point | DC Voltage Limits | Voltage Out of Limits, Check |
| :--- | :---: | :---: |
| Emitter of Q101 | -1.5 to -2.5 | C112, R116, R115, C110, Q101 |
| Collector of Q101 | -4.5 to -6.0 | Q101, C113, R117 to R124 |
| Positive end of C116* | -3.5 to -4.5 | Q103, R132, Q102, C115 |
| * Short base to emitter of Q101 |  |  |

Table 5-7. DC Voltages in Squaring Circuit

| Test Point | DC Voltage Limits | Voltage Out of Limits, Check |
| :--- | :---: | :---: |
| Cathode CR113 | +10.30 to +10.46 | CR113, R167, R173 |
| Cathode CR112 | +8.50 to +9.64 | CR112, R174, R168 |
| Cathode CR111 | +6.41 to +6.51 | CR111, R175, R169 |
| Cathode CR110 | +4.39 to +4.47 | CR110, R176, R170 |
| Cathode CR109 | +2.48 to +2.52 | CR109, R177, R171 |
| Cathode CR108 | 0 | CR108, CR109 to CR113 |

Paragraphs 5-25


Figure 5-2. Top View
b. Using the dc voltmeter, make dc measurements at the points listed in table 5-5. If the presence of 10 kc signal interferes with the dc measurements, the 10 kc oscillator can be disabled, without appreciably affecting the dc voltages, by grounding the collector of Q109. DC voltages are measured with reference to the Model 431B ground.

5-25. STEP 3. If there is no 10 kc output from the oscillator-amplifier proceed as follows:
a. Disconnect the thermistor mount.
b. Disconnect the positive lead of C125 from the circuit board.
c. Make a direct connection between the positive lead of C125 and bridge side of C120 (terminal 35 on the underside of the circuit board).
d. Using the oscilloscope, monitor the output of the oscillator-amplifier. If oscillation is present, the metering and rf bridges should be examined for defect. The waveform of the oscillation under this condition may show limiting.

5-26. If component replacement is required as a result of the foregoing tests, note the following:
a. After replacement of Q110 or Q111, check the amplitude of the 10 kc oscillator-amplifier output (paragraph 5-23a).
b. If Q108 or Q109 has been replaced, check the output frequency of the oscillator-amplifier (para.5-23b).
c. After replacement of L 105 or C 124 , readjustment of the oscillator frequency could be necessary. See paragraph 5-58 for this procedure.

## 5-27. 10 KC AMPLIFIER CHECK.

5-28. A dc voltmeter and oscilloscope are needed for checking the 10 kc amplifier. Table 5-1, Test Equipment, gives equipment requirements. Refer to figure $5-2$, Top View, for component location.
5-29. Table 5-6 lists dc voltage check points and possible causes for deviations from the given limits. All voltages are referenced to the Model 431Bground. If the presence of a $10-\mathrm{kc}$ signal interferes with dc measurement, ground the center tap of L102.
5-30. Calibration inaccuracy, common to all power ranges, can be caused by the 10 kc amplifier. In particular, an out-of-tolerance resistor in the collector of Q101 or a defect in the Q102 stage, which results in improper gain, will produce calibration error.
$5-31$. An open signal path or very low gain in the $10-\mathrm{kc}$ amplifier can drive the meter pointer to its downscale limit. For signal tracing, the 10 kc error signal from the metering bridge can be used, or C110 can be disconnected and used as a means of injecting a substitute 10 kc test signal.

## Note

A special soldering tip is required to replace transformer T102. Refer to table 5-1 for the type of soldering tip to be used.

## 5-32. METERING AND FEEDBACK CIRCUIT.

5-33. Before performing this procedure refer to paragraphs 5-69 and 5-70 and check values of R141 and R179. The differential amplifier (Q104 and Q105), the feedback current squared generator (Q106), the feedback current generator (Q107), and the squaring circuit comprise the metering and feedback circuit. See figure 5-2, top view, for component location.

## Note

Transistors Q106 and Q107 are selected for optimum calibration accuracy. If Q106 or Q107 is replaced, check calibration accuracy using procedure given in paragraph 5-76 or 5-78. It may be necessary to try several transistors to get proper calibration accuracy.

## 5-34. SQUARING CIRCUIT CHECKS.

5-35. A check of the squaring circuit is advisable if full scale or tracking accuracy of the Model 431B does not meet specifications. The squaring circuit includes CR108 through CR113 and R167 through R177. Figure 5-2, Top View, shows component location.

5-36. The squaring circuit is tested under two conditions: (1) when all diodes are conducting, and (2) when no diodes are conducting. Both conditions should be used whenever the squaring circuit is tested.

5-37. A digital voltmeter (see table 5-1) for specifications) is recommended for the following measurements.

5-38. DIODES CONDUCTING. The following procedure measures the forward voltage drop of each diode in the squaring circuit.
a. Set the Model 431B RANGE switch to 1 MW , and adjust the ZERO and VERNIER controls for exact full scale deflection of the meter pointer.
b. Disconnect the grounding link at the digital voltmeter input, and measure the voltage drop across the individual diodes of the squaring circuit. The requirement is 0.4 to 0.5 vdc .

5-39. DIODES OFF. The test points listed in table $5-7$ are the midpoints of five two-resistor voltage dividers connected between -18 vdc and ground. This check verifies that each diode is properly back biased.
a. Adjust the Model 431B ZERO control for a belowzero deflection of the meter pointer.
b. Connect the voltmeter (ungrounded input) between the regulated -18 vdc supply and the test points listed in table 5-7. The voltmeter readings should be within the limits specified in the table.

## 5-40. BATTERY AND CHARGING CHECKS.

$5-41$. The information and procedures which follow pertain to power meters having the optional nickel cadmium battery. The battery is an assembly of 20 individual, permanently sealed cells connected in series. At full charge, battery terminal voltage should be 27 volts $\pm 1$ volt. An inoperative cell reduces terminal voltage by approximately 1.3 volts.

## 5-42. BATTERY CHECK.

5-43. BATTERY VOLTAGE. A de voltmeter is needed for this test. See table 5-1 for voltmeter requirements.
a. Make sure that the Model 431B is disconnected from the ac line. Connect the dc voltmeter between the BATTERY - and BATTERY + terminals on the etched circuit board.
b. Set the POWER switch to BATTERY ON and observe the voltmeter reading. Battery voltage should be -24 to -27 volts. If it is not, and the battery has been charged, check the charging circuits and the current drain imposed by the Model 431B circuitry. If the state of charge of the battery is uncertain, allow a 48 -hour recharge, then recheck the battery voltage. Check the charging circuits if the battery voltage is still not within $27 \pm 1$ volt.

## Paragraphs 5-44 to 5-55

5-44. BATTERY CURRENT DRAIN. The current supplied by the battery to the Model 431B circuitry should be checked if the battery does not seem to maintain a charge. A clip-on or series-connected current meter (see table 5-1) is required for the following procedure.
a. Check that the Model 431B is disconnected from the ac line.
b. Connect the current meter to monitor the current in one of the leads between the battery terminals and the BATTERY - and BATTERY + terminals on the circuit board.
c. Set the POWER switch to BATTERY ON and observe the reading on the current meter; it should read 40 to 53 ma .

## 5-45. CHARGING CHECKS.

$5-46$. The following procedures test the recharge and trickle charge capability of the Model 431B. A direct current meter (see table 5-1), a 7500 ohm $\pm 1 \%$, 2 watt resistor and a $780 \mathrm{ohm} \pm 1 \%, 3$ watt resistor are required for these tests. The battery is disconnected from the BATTERY - and BATTERY + circuit board terminals during both tests.

5-47. TRICKLE CHARGE CURRENT. The following procedure is used to check the trickle charge current applied to the battery when the power meter is operated from ac primary power.
a. Connect the 7500 ohm 2 -watt resistor between the BATTERY - and BATTERY + terminals of the circuit board.
b. Connect the current meter to monitor the current through the resistor.
c. Connect the Model 431B to the ac line, set the POWER switch to AC, and observe the reading of the current meter. Trickle-charge current should be 3.2 to 4.8 ma .

5-48. CHARGE CURRENT. The following procedure checks the current supplied for recharging the battery.
a. Connect the 780 ohm 3 -watt resistor between the BATTERY - and BATTERY + terminals of the circuit board.
b. Connect the current meter to monitor current through the resistor.
c. Connect the Model 431B to the ac line, set the POWER switch to BATTERY CHARGE, and observe the reading of the current meter. Charging current should be 27 to 40 ma .

5-49. A battery which will not assume rated terminal voltage with proper charging current may have a defective cell or cells. In such cases the battery must be replaced (see section VI Table of Replaceable Parts).

5-50. BATTERY WARRANTY.
$5-51$. The warranty, appearing on the inside of the rear cover of this manual, also applies to the accessory battery (option 01 ). Within the warranty period, the battery may be returned to $(\hbar \bar{j})$ Customer Service for repair or replacement.

## 5-52. REPAIR.

5-53. The etched circuit board used in the Model 431B is of the plated-through type which consists of a base board and conductor. The board does not include funneled eyelets. The conductor material is plated to the wall of the holes; thus the conductor is effectively extended into the hole. This type of board can be soldered from either the conductor or component side of the board with equally good results. The rules given below should be followed when repairing a platedthrough type etched circuit board.
a. Avoid applying excessive heat when soldering on the circuit board.
b. To remove a damaged component, clip component leads near the component; then apply heat and remove each lead with a straight upward motion.
c. Use a special tool to remove components having multiple connections, such as potentiometers, transformers, etc. Refer to table 5-1 for type of soldering tip required.
d. Use a toothpick to free hole of solder before installing a new component.

## 5-54. MECHANICAL ADJUSTMENT OF METER ZERO.

5-55. When meter is properly zero-set, pointer rests over the zero calibration mark on the meter scale when the instrument is 1) at normal operating temperature, 2) in its normal operating position, and 3) turned off. Zero-set as follows to obtain best accuracy and mechanical stability:
a. Allow the instrument to operate for at least 20 minutes; this allows the meter movement to reach normal operating temperature.
b. Turn instrument off and allow 30 seconds for all capacitors to discharge.
c. Rotate mechanical zero adjustment screw until pointer is on zero. Reverse direction of adjustment screw approximately $3^{\circ}$ in order to free adjustment screw from meter movement. If the pointer moves while freeing the adjustment screw, this step must be repeated.

## Note

Use of the parallax-eliminating mirror on the meter scale increases the accuracy of the mechanical zero-set.

## 5-56. ADJUSTMENTS.

## 5-57. POWER SUPPLY ADJUSTMENT.

a. Connect a dc voltmeter (see table 5-1 for required specifications) between the negative end of C6 and Model 431B ground.
b. Adjust -18 v REG. ADJ., R13, for -18 vdc.
c. Vary line voltage from 103 to $127 \mathrm{vac}(207$ to 253 vac): -18 vdc should not vary perceptibly.

## 5-58. OSCILLATOR FREQUENCY ADJUSTMENT.

5-59. If both 100 and 200 ohm thermistor mounts are to be used interchangeably with the Model 431B, the frequency of the 10 kc oscillator-amplifier should be adjusted in the following sequence: the 200 ohm mount procedure, paragraph 5-61, then the 100 ohm mount procedure, paragraph 5-62. If only one type of mount will be used with the power meter only the appropriate procedure is required.

5-60. An oscilloscope and frequency counter are needed for these adjustments. See table 5-1, Test Equipment for requirement. A plastic alignment tool should be used for the adjustment of L101 to avoid core damage.

5-61. 200 OHM MOUNT. The following procedure adjusts the 10 kc oscillator frequency when a 200 ohm thermistor mount is connected to the Model 431 B .
a. Connect the $200 \Omega$ thermistor mount and cable to the Model 431B; set the MOUNT RES switch to $200 \Omega$.
b. Connect the frequency counter between the plus end of C125 and ground; adjust L101 to give a frequency of $10,150 \mathrm{cps}$.
c. Connect the oscilloscope to the base of Q108 and observe the feedback signal amplitude. It should not exceed 12 mv peak-to-peak.

5-62. 100 OHM MOUNT. The following procedure adjusts the 10 kc oscillator frequency when a 100 ohm thermistor mount is connected to the Model 431B.
a. Connect the 100 ohm thermistor mount and cable to the Model 431B, and set MOUNT RES to $100 \Omega$.
b. Connect the frequency counter between the positive end of C125 and ground. The frequency should be $10 \mathrm{KC} \pm 50 \mathrm{cps}$. If it is not, proceed with step c .
c. Substitute values of capacitance for C101 until the frequency is within the limits of step b.

## Note

A decade capacitance box can be used to determine proper value of capacitance that must be used (see table 5-1).

## 5-63. COARSE NULL ADJUSTMENT.

$5-64$. If both 100 and 200 ohm thermistor mounts are to be used interchangeably with the Model 431B, the coarse null adjustment should be made in the following sequence; the procedure in paragraph 5-67 first, and then the procedure in paragraph 5-68.
$5-65$. If only a 200 ohm thermistor mount is to be used with the power meter, follow the procedure of paragraph 5-68. When only a 100 ohm thermistor mount is to be used, the procedure of paragraph $5-67$ is sufficient.

5-66. An oscilloscope or ac vtvm is needed for these adjustments. See table 5-1, Test Equipment, for requirements. A plastic alignment tool should be used for the adjustment of L102 to avoid core damage.
$5-67$. 100 OHM MOUNT. The following procedure is used to make coarse adjustment of the null when a 100 ohm thermistor mount is connected to the Model 431B.
a. Set MOUNT RES to $100 \Omega$.
b. Observe the arrangement and travel of null capacitor C103, then mechanically center C103.
c. Connect the oscilloscope or ac vtvm between ground and the base of Q103.
d. Switch the Model 431B on and set RANGE to 10 MW .
e. Adjust the ZERO control to maintain a meter indication of less than $5 \%$ of full scale on the Model 431B while adjusting L102 for a minimum indication on the oscilloscope or vtvm.
f. Set RANGE to .01 MW and repeat step e, this time maintaining an on-scale meter indication on the Model 431B.
g. Move the oscilloscope or vtvm connection from the base of Q103 to the lead of R138 nearest T103.
h. Adjust null capacitor C103 to minimize the oscilloscope or vtvm indication. Minimum indication should occur with the capacitor near the center of its range.

## Note

A decade capacitance box can be used to determine the value of capacitance to be added (refer to table 5-1).
i. Set Model 431B RANGE switch to NULL. Adjust the null capacitor, C103, for a minimum indication on the Model 431B meter. Minimum indication should occur at less than $4 \%$ of full scale and C103 should be near its mid-range.

5-68. 200 OHM. The following procedure is used to make coarse null full adjustment when a 200 ohm thermistor mount is connected to the Model 431B.
a. Set MOUNT RES to $200 \Omega$.
b. Set RANGE to .01 MW .
c. Connect the oscilloscope or vtvm between ground and the lead of R138 nearest T103.
d. Mechanically center the null capacitor, C103, by observing its rotor plates.
e. Using the ZERO and VERNIER controls, maintain an on-scale indication on the Model 431B meter while substituting values for C105 to obtain a minimum indication on the oscilloscope or vtvm.
f. Adjust C103, the null capacitor, to improve the minimum indication on the oscilloscope or vtvm. The null capacitor should be near mid-range.

## Note

A decade capacitance box can be used to determine the value of capacitance to be added (see table 5-1).
g. Set RANGE to NULL. The Model 431B meter deflection should be less than $4 \%$ of full scale. If it is not, increase the value of C 104 in approximately 50 pf increments to a maximum value of 500 pf . If 100 and 200 ohm thermistor mounts are to be used, repeat the null procedure for 100 ohm mounts (paragraph 5-67) after each increase in capacitance of C104.

5-69. ZERO AND VERNIER CONTROL ADJUSTMENT.
a. Connect a dc digital voltmeter (see table 5-1) at the Model 431B RECORDER jack. Use a special telephone-plug-to-dual-banana-plug cable assembly terminated with a $1000-\mathrm{ohm} \pm 0.1 \%$ 0.25 -watt wirewound resistor.
b. Set Model 431B RANGE to . 01 MW , and adjust Model 431B ZERO and VERNIER controls for zero meter reading on the Model 431B.
c. Set Model 431 B RANGE to 10 MW .
d. Connect a decade resistance box across R141 (see figure 5-2), and adjust to obtain zero indication on Model 431B Power Meter.
e. Note amount of resistance required from resistance box to obtain zero indication.
f. Remove the decade resistance box, and replace with resistor of value noted in step $e$.
g. Check the Model 431B range-to-range zero drift by 1) setting Model 431B RANGE to .01 MW , and readjusting its VERNIER for zero meter reading, 2) switching the Model 431B through its complete range while observing the digital dc voltmeter reading. Test limits: digital dc voltmeter reading must not exceed $+5 \mathrm{mv}(+0.005 \mathrm{~V})$ on any Model 431B range.

## 5-70. FULL SCALE ACCURACY ADJUSTMENT.

a. Connect a $b$ Model 8402A (see table 5-1) at the Model 431B POWER METER terminals. Check that Model 8402A OUTPUT CURRENT is off.
b. Set Model 431B RANGE to 10 MW ; set Model 8402A RANGE (MW) to 10 MW , and FUNCTION to CAL.
c. Adjust the Model 431B ZERO and VERNIER controls for a zero indication on the meter.
d. Set Model 8402A OUTPUT CURRENT to ON; note and record the Model 431B percent-of-powerreading error.
e. Set Model 8402A OUTPUT CURRENT to off.
f. Set Model 431B RANGE to 3 MW ; set Model 8402A RANGE (MW) to 3 MW .
g. Reset Model 431B VERNIER to zero the meter, if necessary.
h. Set Model 8402A OUTPUT CURRENT to ON; note and record the Model 431B percent-of-powerreading error ( $1.7 \%$ /division on $0-3$ meter scale).
i. Repeat steps b through h for all Model 431B RANGE positions.
j. Connect a decade resistance box across R179 (see figure 5-2).
k. Select the resistance value which equalizes the magnitude of the largest positive and negative percent error.
m. Remove the decade resistance box, and replace with a resistor of the value selected in step $k$.
n. Check all Model 431B RANGE positions. Test limits. The Model 431B full-scale power-reading error must not exceed $1-1 / 2 \%$ on all range positions.

## Note

When only a 100 ohm thermistor mount will be used with the Model 431B, the value of C104 may be changed to obtain the null requirements specified above.

## 5-71. PERFORMANCE CHECK.

$5-72$. The tests described below which verify that the Model 431 B meets specifications, use only panel controls and connectors. These tests can be used for incoming quality control, for routine preventive maintenance, and after repair. A thermistor mount must be connected to the Model 431B for the performance checks, though no rf power will be applied.

## Note

If there is possibility of rf pick-up, the thermistor mount should be appropriately shielded.

5-73. Check the mechanical zero-set of the Model 431B meter according to paragraph 5-54.

5-74. ZERO CARRY-OVER CHECK.
a. Set Model 431B RANGE to . 01 MW.
b. Adjust ZERO and VERNIER controls to set the meter pointer over the zero calibration mark.
c. Rotate RANGE through its .03, .1, .3, and 10 MW positions, observing the accuracy of the zero setting at each position. The zero must carry over from range to range within $\pm 1 \%$ of full scale.

## 5-75. CALIBRATION AND RANGE TRACKING ACCURACY.

5-76. Calibration and range tracking accuracy is verified by dc substitution. Briefly, dc substitution involves 1) applying enough direct current at the DC CALIBRATION \& SUBSTITUTION terminals to obtain the desired meter indication 2) accurately determining the applied current and 3) calculating the dc power applied. The difference between the substituted dc power and the meter indication it produced is the calibration error. The Model 8402A Power Meter Calibrator, or other means of producing accurate direct currents, is used as the substitution source.

5-77. CALIBRATION AND TRACKING ACCURACY TEST USING THE 扁 MODEL 8402A POWER METER CALIBRATOR. The Model 8402A Power Meter Calibrator provides constant currents sufficient to cause full scale meter indication on each of the Model 431B power ranges. It also has provision for checking the tracking accuracy of the Model 431B on the 10 mw range.

5-78. Refer to the Operating and Service Manual of the Power Meter Calibrator for correct test procedure.

5-79. ALTERNATE METHOD FOR CHECKING CALIBRATION AND RANGE TRACKING ACCURACY. The calibration and range tracking accuracy of the Model 431B can be checked by dc substitution using the equipment and connections shown in figure 3-3.
$5-80$. Using the data in table $5-8$ the full scale calibration accuracy of each range and the tracking accuracy of the 10 mw range can be tested.

Table 5-8. Data for Calibration, Tracking Accuracy Check

| Test Point |  | Substitution Current ( $\mathrm{Idc}_{\text {c }}$ ) |  | Model 431B Meter Reads |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Full } \\ & \text { Scale } \end{aligned}$ | Tracking | $\begin{gathered} \text { Mount Res } \\ 100 \Omega \end{gathered}$ | $\begin{gathered} \text { Mount Res } \\ 200 \Omega \end{gathered}$ |  |
| 10 mw |  | 20.00 ma | 14.14 ma | 9.7 to 10.3 mw |
|  | 8 mw | 17.89 | 12.65 | 7.76 to 8.24 mw |
|  | 6 mw | 15.49 | 10.95 | 5.82 to 6.18 mw |
|  | 4 mw | 12.65 | 8.94 | 3.88 to 4.12 mw |
|  | 2 mw | 8.94 | 6.32 | 1.94 to 2.06 mw |
| 3 mw |  | 10.95 | 7.75 | 2.91 to 3.09 mw |
| 1 mw |  | 6.32 | 4.47 | 0.97 to 1.03 mw |
| .3 mw |  | 3.46 | 2.45 | 0.291 to 0.309 mw |
| .1 mw |  | 2.00 | 1.41 | 0.097 to 0.103 mw |
| . 03 mw |  | 1.10 | 0.775 | 0.0291 to 0.0309 mw |
| . 01 mw |  | 0.632 | 0.447 | 0.0097 to 0.0103 mw |



WAVEGUIDE THERMISTOR
MOUNT
4864




## SECTION VI <br> REPLACEABLE PARTS

## 6-1. INTRODUCTION.

6-2. This section contains information for ordering replacement parts. Table 6-1 lists parts in alphanumerical order of their reference designators and indicates the description and $(b)$ stock number of each part, together with any applicable notes. Table 6-2 lists parts in alpha-numerical order of their (b) stock numbers and provides the following information on each part:
a. Description of the part (see list of abbreviations below).
b. Typical manufacturer of the part in a five-digit code; see list of manufacturers in appendix.
c. Manufacturer's stock number.
d. Total quantity used in the instrument (TQ column).
e. Recommended spare part quantity for complete maintenance during one year of isolated service (RS column).

6-3. Miscellaneous parts not indexed in table 6-1 are listed at the end of table 6-2.

## 6-4. ORDERING INFORMATION.

6-5. To order a replacement part, address order or inquiry either to your authorized Hewlett-Packard sales representative or to

CUSTOMER SERVICE<br>Hewlett-Packard Company<br>395 Page Mill Road<br>Palo Alto, California

or, in Western Europe, to
Hewlett-Packard S.A.
54-54bis Route des Acacias
Geneva, Switzerland
6-6. Specify the following information for each part:
a. Model and complete serial number of instrument.
b. Hewlett-Packard stock number.
c. Circuit reference designator.
d. Description.

6-7. To order a part not listed in tables 6-1 and 6-2, give a complete description of the part and include its function and location.

REFERENCE DESIGNATORS

| A | $=$ assembly |
| :--- | :--- |
| B | $=$ motor |
| C | $=$ capacitor |
| CR | $=$ diode |
| DL | $=$ delay line |
| DS | $=$ device signaling (lamp) |
| $\mathbf{E}$ | $=$ misc electronic part |


|  | amperes |
| :---: | :---: |
|  | bandpass |
| BWO | = backward wave oscillator |
| CER | = ceramic |
| CMO | = cabinet mount only |
| COEF= | = coefficient |
| COM $=$ | = common |
| COMP= | = composition |
| CONN= | = connection |
| CRT | = cathode-ray tube |

DEPC= deposited carbon
EIA $=$ Tubes or transistors meeting Electronic Industries' Association standards will normally result in instrument operating within specifications; tubes and transistors selected for best performance will be supplied if ordered by 47 stock numbers.
ELECT = electrolytic
ENCAP = encapsulated

| F | $=$ fuse |
| :--- | :--- |
| FL | $=$ filter |
| $\mathbf{J}$ | $=$ jack |
| $\mathbf{K}$ | $=$ relay |
| $\mathbf{L}$ | $=$ inductor |
| $\mathbf{M}$ | $=$ meter |
| $\mathbf{M P}$ | $=$ mechanical part |

P = plug
Q = transistor
R = resistor

## RT = thermistor

S $=$ switch
T = transformer
ABBREVIATIONS

| F | farads | NC $=$ normally closed |
| :--- | :--- | :--- |
| FXD | $=$ fixed | NE |

HG = mercury : replaceable

OBD = order by description

P = peak
PC = printed circuit board
PF = picofarads =
PP = peak-to-peak
PIV = peak inverse voitage
POR = porcelain
POS = position(s)
POLY = polystyrene
POT = potentiometer
RECT $=$ rectifier
ROT $=$ rotary
RMS = root-mean-square
RMO = rack mount only

| $\mathbf{V}$ | $=$ vacuum tube, neon |
| :--- | :--- |
| bulb, photocell, etc. |  |
| $\mathbf{W}$ | $=$ cable |
| $\mathbf{X}$ | $=$ socket |
| $\mathbf{X F}$ | $=$ fuseholder |
| $\mathbf{X D S}$ | $=$ lampholder |
| $\mathbf{Z}$ | $=$ network |


| $\begin{aligned} & \text { S-B } \\ & \text { SE } \end{aligned}$ | $\begin{aligned} & \text { = slow -blow } \\ & =\text { selenium } \end{aligned}$ |
| :---: | :---: |
| SECT | = section(s) |
| SI | = silicon |
| SIL | = silver |
| SL | = slide |
| TA | = tantalum |
| TD | = time delay |
| TI | = titanium dioxide |
| TOG | $=$ toggle |
| TOL | = toleranc |
| TRIM | $=$ trimmer |
| TWT | = traveling wave tube |
| U | $=$ micro $=10^{-6}$ |
| VAC | = vacuum |
| VAR | = variable |
| W/ | $=$ with |
| W | = watts |
| WW | = wirewound |
| W/o | without |
| * | = optimum value selected at factory, average value shown (part may be omitted) |
| \% | = number |

Table 6-1. Index by Reference Designator

| Circuit Reference | (tp) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| A101 | 431B-65A | Assy, etched circuit, includes: |  |
|  |  | C1 thru C6 R102, R103 |  |
|  |  | C102, C106 R105 thru R110 |  |
|  |  | C110 thru C125 R113 thru R116 |  |
|  |  | CR1 thru CR9 R125 thru R140 |  |
|  |  | CR101 thru CR113 R142 thru R144 |  |
|  |  | L101 thru L105 R150 thru R155 |  |
|  |  | Q1 thru Q5 R167 thru R178 |  |
|  |  | Q101 thru Q111 R180 |  |
|  |  | R2 thru R7 Z1 |  |
|  |  | R9 thru R14 |  |
| BT1 |  | See Option 01 |  |
| C1 | 0180-0049 | C: fxd, aluminum elect, $20 \mu \mathrm{f}, 50$ vdcw |  |
| C2 | 0180-0138 | C: fxd, aluminum elect, $100 \mu \mathrm{f}+100 \%-10 \%, 40$ vdew |  |
| C3 | 0150-0012 | C: fxd, cer, $0.01 \mu \mathrm{f} \pm 20 \%, 1000$ vdcw |  |
| C4 | 0160-0174 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%-20 \%, 25 \mathrm{vdcw}$ |  |
| C5 | 0180-0059 | C: fxd, elect, $10 \mu \mathrm{f}+100 \%-10 \%$, 25 vdew |  |
| C6 | 0180-0105 | C: fxd, aluminum elect, $50 \mu \mathrm{f}, 25$ vdew |  |
| C7 thru C100 |  | Not assigned |  |
| C101 | 0140-0220 | C: fxd, mica, 200*pf $\pm 1 \%, 300 \mathrm{vdcw}$ |  |
| C102 | 0160-0185 | C: fxd, mica, 2100pf $\pm 1 \%, 300$ vdcw |  |
| C103 | 0121-0035 | C: var, air, 7.2-143.7pf |  |
| C104 | 0140-0204 | C: fxd, mica, $47 *$ pf $\pm 5 \%, 500$ vdew |  |
| C105 | 0140-0220 | C: fixd, mica, $200 *$ pf $\pm 1 \%, 300$ vdcw |  |
| C106 | 0180-0106 | C: fxd, tantalum elect, $60 \mu \mathrm{f} \pm 20 \%, 6$ vdew |  |
| C107 thru C109 |  | Not assigned |  |
| C110 | 0160-0174 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%$ |  |
| C111 | 0180-0059 | C: fxd, elect, $10 \mu \mathrm{f}+100 \%-10 \%, 25$ vdew |  |
| C112 | 0170-0069 | C: fxd, poly, $0.1 \mu \mathrm{f} \pm 2 \%, 50$ vdcw |  |
| C113 | 0160-0174 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%-20 \%$, 25 vdcw |  |
| C114 | 0180-0059 | C: fxd, elect, $10 \mu \mathrm{f}+100 \%-10 \%, 25$ vdcw |  |
| C115 | 0170-0069 | C: fxd, poly, $0.1 \mu \mathrm{f} \pm 2 \%, 50 \mathrm{vdcw}$ |  |
| C116 | 0180-0059 | C: fxd, elect, $10 \mu \mathrm{f}+100 \%-10 \%, 25 \mathrm{vdcw}$ |  |
| C117 | 0160-0105 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%-20 \%, 25$ vdcw |  |
| C118, C119 | 0180-0105 | C: fxd, aluminum elect, $50 \mu \mathrm{f}, 25 \mathrm{vdcw}$ |  |

Table 6-1. Index by Reference Designator (Cont'd)

| Circuit <br> Reference | (50) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| C120 | 0160-0174 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%-20 \%, 25$ vdcw |  |
| C121, C122 | 0180-0059 | C: fxd, elect, $10 \mu \mathrm{f}+100 \%-10 \%$, 25 vdcw |  |
| C123 | 0160-0174 | C: fxd, cer, $0.47 \mu \mathrm{f}+80 \%-20 \%, 25 \mathrm{vdcw}$ |  |
| C124 | 0170-0069 | C: fxd, poly, $0.1 \mu \mathrm{f} \pm 2 \%, 50 \mathrm{vdcw}$ |  |
| C125 | 0180-0049 | C: fxd, aluminum elect, $20 \mu \mathrm{f}, 50$ vdcw |  |
| CR1 thru CR4 | 1901-0025 | Diode, Si: 50 ma @+1V, 100 PIV |  |
| CR5, CR6 | 1901-0026 | Diode, Si |  |
| CR7 | 1902-0017 | Diode, St: avalanche |  |
| CR8 | 1902-0018 | Diode, Si: avalanche, 1N941 |  |
| CR9 | 1902-0017 | Diode, Si: avalanche |  |
| CR10 thru CR100 |  | Not assigned |  |
| CR101 thru CR104 | 1910-0016 | Diode, Ge: $100 \mathrm{ma} @ 1 \mathrm{~V}, 60 \mathrm{PIV}$ |  |
| CR105, CR106 | 1901-0025 | Diode, St: $50 \mathrm{ma} @+1 \mathrm{~V}, 100 \mathrm{PIV}$ |  |
| CR107 thru CR113 | 1901-0024 | Diode, SH |  |
| DS1 | 1450-0048 | Lamp, Ne: NE2H |  |
| F1 | 2100-0017 | Fuse, cartridge: 0.15 amp |  |
| J1 | 1251-0148 | Connector, POWER: male, 3 pin |  |
| J2 thru J100 |  | Not assigned |  |
| J101 | 1251-0149 | Connector, female, 6 contact |  |
| J102 | 1251-0066 | Jack, telephone, for 2 connector plug |  |
| J103 | AC-10C | DC CALIBRATION and SUBSTITUTION, consists of Binding post: black |  |
|  | AC-10D | Binding post: red |  |
|  | AC-54A | Insulator: black, 2 hole (inside) |  |
|  | AC-54A-1 | Insulator: black, 2 hole (outside) |  |
| L1 |  | Nsr: part of Z1 |  |
| L2 thru L100 |  | Not assigned |  |
| L101, L102 | 9140-0122 | Coil, var, 2 windings, $9-20 \mu \mathrm{~h}$ each |  |
| L103 thru L105 | 9110-0040 | Inductor, audio, 2.5 mh |  |
| M1 thru M100 |  | Not assigned |  |
| M101 | 431B-81A | Meter, calibrated |  |

Table 6-1. Index by Reference Designator (Cont'd)

| Circuit Reference | (迆) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| P1 |  | Nsr; prat of W1 |  |
| P2 |  | Nsr; part of W1 |  |
| Q1 | 1850-0065 | Transistor, Ge: 2 N 1370 |  |
| Q2 | 1850-0064 | Transistor: 2N1183 |  |
| Q3 | 1850-0065 | Transistor: Ge, 2N1370 |  |
| Q4 | 1851-0017 | Transistor, Ge: 2N1304 |  |
| Q5 | 1854-0003 | Transistor, Si |  |
| Q1 thru Q100 |  | Not assigned |  |
| Q101 | 1850-0065 | Transistor: Ge, 2N1370 |  |
| Q102 | 1851-0017 | Transistor, Ge: 2N1304 |  |
| Q103 thru Q105 | 1850-0065 | Transistor, Ge: 2N1370 |  |
| Q106, Q107 | 1854-0003 | Transistor, Si |  |
| Q108 | 1850-0065 | Transistor, Ge: 2N 1370 |  |
| Q109 | 1851-0017 | Transistor, Ge: 2N1304 |  |
| Q110 | 1850-0040 | Transistor: 2N383 |  |
| Q111 | 1851-0017 | Transistor, Ge: 2N1304 |  |
| R1 | 0687-3331 | R: fxd, comp, 33 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R2 | 0687-3321 | R: fxd, comp, 3.3K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R3 | 0690-3911 | R : fxd, comp, 390 ohms $\pm 10 \%, 1 \mathrm{~W}$ |  |
| R4 | 0690-1221 | R: fxd, comp, 1.2 K ohms $\pm 10 \%$, 1W |  |
| R5 | 0687-4721 | R : fxd, comp, 4.7 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R6 | 0687-2711 | R: fxd, comp, 270 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R7 | 0687-3321 | R: fxd, comp, 3.3 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R8 |  | Nsr; part of Z1 |  |
| R9 | 0687-4721 | R: fxd, comp, 4.7K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R10 | 0687-3321 | R: fxd, comp, 3.3K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R11 | 0687-1821 | R: fxd, comp, 1.8K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R12 | 0758-0006 | R : fxd, metallic oxide, 10 K ohms $\pm 5 \%, 0.5 \mathrm{~W}$ |  |
| R13 | 2100-0182 | R : var, comp, lin, 3.3 K ohms $\pm 10 \%, 1 / 3 \mathrm{~W}$ |  |
| R14 | 0758-0005 | R : fxd, metallic oxide, 4.7 K ohms $\pm 5 \%, 0.5 \mathrm{~W}$ |  |
| R15 thru R100 |  | Not assigned |  |
| R101 | 0727-0395 | R: fxd, dep c, 316 ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| Option 10 | 0727-0483 | R: fxd, dep $c, 318.1$ ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| Option 11 | 0727-0484 | R : fxd, dep c, 320.1 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| Option 12 | 0727-0485 | R : fxd, dep c, 323.4 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |

Table 6-1. Index by Reference Designator (Cont'd)

| Circuit Reference | (tap) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| Option 21-23 | 0727-0486 | R: fxd, dep c, 329.8 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| R102 | 0811-0051 | R: fxd, ww, 200.3 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 10 | 0811-0100 | R : fxd, ww, 200.7 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 11, 21 | 0811-0085 | R: fxd, ww, 202.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 12, 22 | 0811-0086 | R: fxd, ww, 204.3 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 13,23 | 0811-0087 | R: fxd, ww, 208.8 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| R103 | 0811-0051 | R: fxd, ww, 200.3 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 10 | 0811-0099 | R: fxd, ww, 202.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 11, 21 | 0811-0088 | R: fxd, ww, 206.6 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 12, 22 | 0811-0089 | R: fxd, ww, 213.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 13, 23 | 0811-0090 | R: fxd, ww, 227.6 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ |  |
| R105 | 0811-0063 | R: fxd, ww, 189 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 10 | 0811-0094 | R: fxd, ww, 190.9 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 11, 21 | 0811-0095 | R: fxd, ww, 194.2 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ |  |
| Option12, 22 | 0811-0096 | R: fxd, ww, 200.7 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ |  |
| Option 13, 23 | 0811-0101 | R: fxd, ww, 212.7 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ |  |
| R106 | 0811-0064 | R: fxd, ww, 255 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ |  |
| Option 10 | 0811-0091 | R: fxd, ww, 256 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ |  |
| Option 11, 21 | 0811-0098 | R: fxd, ww, 258.2 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ |  |
| Option 12, 22 | 0811-0092 | R: fxd, ww, 262.1 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ |  |
| Option 13, 23 | 0811-0093 | R: fxd, ww, 265.5 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ |  |
| R107 | 0811-0065 | R: fxd, ww, 511 ohms $\pm 1 \%, 0.08 \mathrm{~W}$ |  |
| R108 | 0811-0066 | R: fxd, ww, 887 ohms $\pm 1 \%, 0.08 \mathrm{~W}$ |  |
| R109 | 0758-0020 | R : fxd, $\mathrm{mfgl}, 22 \mathrm{~K}$ ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R110 | 0811-0065 | R: fxd, ww, 511 ohms $\pm 1 \%, 0.08 \mathrm{~W}$ |  |
| R111A/B | 2100-0342 | $R$ : var, concentric <br> Front sect: ww, lin, 10 K ohms $\pm 10 \%, 2 \mathrm{~W}$ <br> Rear sect: $\mathrm{ww}, \mathrm{lin}, 800 \mathrm{ohms} \pm 10 \%, 2 \mathrm{~W}$ |  |
| R112 |  | Not assigned |  |
| R113 | 0686-7525 | R : fxd, comp, 7.5 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R114 | 0686-3325 | R: fxd, comp, 3.3 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R115 | 0686-2725 | R: fxd, comp, 2.7K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R116 | 0686-3325 | R : fxd, comp, 3.3K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R117 | 0683-4315 | R: fxd, comp, 430 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R118 | 0683-3305 | R: fxd, comp, 33 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R119 | 0683-7505 | R: fxd, comp, 75 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |

\# See introduction to this section

Table 6-1. Index by Reference Designator (Cont'd)

| Circuit <br> Reference | (59) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| R120 | 0683-2215 | R : fxd, comp, 220 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R121 | 0683-1025 | R : fxd, comp, 1 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R122 | 0683-2435 | R : fxd, comp, 24 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R123 | 0683-9115 | R : fxd, comp, 910 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R124 | 0683-2725 | R: fxd, comp, 2.7 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ |  |
| R125 | 0686-1025 | R: fxd, comp, 1 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R126 | 0686-1525 | R: fxd, comp, 1.5 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R127 | 0686-7525 | R: fxd, comp, 7.5 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R128 | 0686-3325 | R : fxd, comp, 3.3 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R129 | 0686-1535 | R: fxd, comp, 15 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R130 | 0687-3321 | R : fxd, comp, 3.3 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R131 | 0687-5611 | R : fxd, comp, 560 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R132 | 0686-3325 | R : fxd, comp, 3.3 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R133 | 0687-1511 | R : fxd, comp, 150 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R134 thru R137 | 0758-0003 | R: fxd, mfgl, 1 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R138 | 0687-1521 | R : fxd, comp, 1.5 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R139 | 0687-1531 | R : fxd, comp, 15 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R140 | 0686-1025 | R : fxd, comp, 1 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R141 | 0687-3931 | R: fxd, comp, 39 K *ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R142 | 0687-1221 | R: fxd, comp, 1.2K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R143, R144 | 0687-5611 | R: fxd, comp, 560 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R145 thru R149 |  | Not assigned |  |
| R150 | 0727-0131 | R: fxd, $\operatorname{dep} \mathrm{c}, 3920$ ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| R151 | 0687-3321 | R : fxd, comp, 3. 3 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R152, R153 | 0727-0124 | R : fxd, dep c, 3 K ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| R154 | 0687-5611 | R: fxd, comp, 560 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R155 | 0687-3311 | R : fxd, comp, 330 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R156 thru R159 |  | Not assigned |  |
| R160 | 0727-0396 | R: fxd, dep c, 1.194 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R161 | 0727-0397 | R: fxd, dep c, 2.13 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R162 | 0727-0398 | R: fxd, dep c, 3.79 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R163 | 0727-0399 | R: fxd, dep c, 6.73 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R164 | 0727-0341 | R : fxd, dep c, 12 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |

Table 6-1. Index by Reference Designator (Cont'd)

| Circuit <br> Reference | (tip) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| R165 | 0727-0400 | R: fxd, dep c, 21.36 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R166 | 0727-0342 | R: fxd, dep c, 38.05 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R167 | 0727-0407 | R: fxd, dep c, 82.09 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R168 | 0727-0346 | R: fxd, dep c, 63.14 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R169 | 0727-0404 | R: fxd, dep c, 52.55 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R170 | 0727-0402 | R: fxd, dep c, 46.67 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R171 | 0727-0401 | R: fxd, dep c, 41.46K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R172 | 0727-0403 | R: fxd, dep c, 52.3 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R173 | 0727-0405 | R : fxd, dep c, 57.46 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R174 | 0727-0406 | R: fxd, dep $c, 69.49 \mathrm{~K}$ ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R175 | 0727-0408 | R: fxd, dep c, 94.2 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R176 | 0727-0409 | R : fxd, dep c, 142 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R177 | 0727-0410 | R : fxd, dep c, 256.8 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ |  |
| R178 | 0687-5631 | R : fxd, comp, 56 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R179 | 0687-5631 | R : fxd, comp, $56 \mathrm{~K} *$ ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ |  |
| R180 | 0758-0021 | $\mathrm{R}: \mathrm{fxd}, \mathrm{mfgl}, 51 \mathrm{~K}$ ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ |  |
| R181 | 0727-0100 | R : fxd, dep c, 1 K ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ |  |
| S1 | 3101-0033 | Switch, sl: DPDT |  |
| S2 | 3100-0370 | Switch, rot: 1 sect, 4 pos, includes: 431B-16C |  |
| S3 thru S100 |  | Not assigned |  |
| S101 | 3101-0032 | Switch, sl: 4PDT |  |
| S102 | 3100-0273 | Switch, rot: 3 sect, 8 pos, includes: $431 \mathrm{~B}-16 \mathrm{~B}$ |  |
| T1 | 9100-0141 | Transformer, power |  |
| T2 thru T100 |  | Not assigned |  |
| T101, T102 | 9120-0066 | Transformer, audio |  |
| T103, T104 | 9120-0065 | Transformer, audio |  |
| W1 | 8120-0078 | Assy, power cable: smooth black, extra limp, 7.5ft. NEMA plug-in |  |
| XF1 | 1400-0084 | Fuseholder: extractor post type |  |
| Z1 | 413A-60A | Assy, coil, includes: L1, R8 |  |

Table 6-1. Index by Reference Designator (Cont'd)


Table 6-1. Index by Reference Designator (Cont'd)

| Circuit Reference | (top) Stock No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
|  |  | OPTIONS |  |
|  | $\begin{aligned} & 1420-0009 \\ & 431 \mathrm{~A}-64 \mathrm{~A} \\ & 431 \mathrm{~A}-64 \mathrm{~B} \\ & 431 \mathrm{~B}-95 \mathrm{~A} \end{aligned}$ | Option 01 <br> Battery, rechargeable (BT1) <br> Support, battery <br> Cover, battery <br> Rechargeable battery installation kit |  |
|  | $\begin{aligned} & 431 \mathrm{~A}-16 \mathrm{G} \\ & 1251-0149 \end{aligned}$ | Option 02 <br> Assy, cable, special purpose includes: Connector, female |  |
|  | 431B-16D | Option 10 <br> Assy, cable $20^{\prime}$ THERMISTOR MOUNT for use with (19) Model 486A or 478A thermistor mount |  |
|  | 431B-16E | Option 11 <br> Assy, cable 50' THERMISTOR MOUNT for use with $(40)$ Model 486A thermistor mount |  |
|  | 431B-16F | Option 12 <br> Assy, cable $100^{\prime}$ THERMISTOR MOUNT for use with (40) Model 486A thermistor mount |  |
|  | 431B-16G | Option 13 <br> Assy, cable 200' THERMISTOR MOUNT for use with (40) Model 486A thermistor mount |  |
|  | 431B-16E | Option 21 <br> Assy, cable 50' THERMISTOR MOUNT for use with (190) Model 478A thermistor mount |  |
|  | 431B-16F | Option 22 <br> Assy, cable 100' THERMISTOR MOUNT for use with (102) Model 478A thermistor mount |  |
|  | 431B-16G | Option 23 <br> Assy, cable 200' THERMISTOR MOUNT for use with ( 40 Model 478A thermistor mount |  |

Table 6-2. Replaceable Parts


Table 6-2. Replaceable Parts (Cont'd)


Table 6-2. Replaceable Parts (Cont'd)

| (5) Stock No. | Description \# | Mfr. | Mfr. Part No. | TQ | RS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0180-0138 | C: fxd, aluminum elect, $100 \mu \mathrm{f}$ $+100 \%-10 \%$, 40 vdcw | 56289 | Type 41D | 1 | 1 |  |
| 0510-0123 | Retainer, indicator light used w/1450-0048 | 78553 | C12008-014-4 | 1 | 0 |  |
| 0683-1025 | R: fxd, comp, 1 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB1025 | 1 | 1 |  |
| 0683-2215 | R: fxd, comp, 220 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB2215 | 1 | 1 |  |
| 0683-2435 | R: fxd, comp, 24 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB2435 | 1 | 1 |  |
| 0683-2725 | R : fxd, comp, 2.7 K ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB2725 | 1 | 1 |  |
| 0683-3305 | R : fxd, comp, $33 \mathrm{ohms} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB3305 | 1 | 1 |  |
| 0683-4315 | R: fxd, comp, 430 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB4315 | 1 | 1 |  |
| 0683-7505 | R: fxd, comp, 75 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB7505 | 1 | 1 |  |
| 0683-9115 | R: fxd, comp, 910 ohms $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 01121 | CB9115 | 1 | 1 |  |
| 0686-1025 | R: fxd, comp, 1 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1025 | 2 | 1 |  |
| 0686-1525 | R: fxd, comp, 1.5 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1525 | 1 | 1 |  |
| 0686-1535 | R: fxd, comp, 15 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1535 | , | 1 |  |
| 0686-2725 | R: fxd, comp, 2.7 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB2725 | 1 |  |  |
| 0686-3325 | R: fxd, comp, 3.3 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB3325 | 4 | , |  |
| 0686-7525 | R: fxd, comp, 7.5 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB2725 | 2 | 1 |  |
| 0687-1221 | R : fxd, comp, $1.2 \mathrm{~K} \mathrm{ohms} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1221 | 1 | 1 |  |
| 0687-1511 | R: fxd, comp, 150 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1511 | 1 | 1 |  |
| 0687-1521 | R: fxd, comp, 1.5 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1521 | 1 | 1 |  |
| 0687-1531 | R: fxd, comp, 15 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1531 | 1 | 1 |  |
| 0687-1821 | R: fxd, comp, 1.8 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB1821 | 1 |  |  |
| 0687-2711 | R: fxd, comp, 270 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB2711 | 1 | 1 |  |
| 0687-3311 | R: fxd, comp, 330 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB3311 | 1 | 1 |  |
| 0687-3321 | R: fxd, comp, $3.3 \mathrm{Kohms} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB3321 | 5 | 2 |  |
| 0687-3331 | R: fxd, comp, 33 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB3331 | 1 | 1 |  |
| 0687-3931 | R: fxd, comp, 39 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB3931 | 1 | 1 |  |
| 0687-4721 | R: fxd, comp, 4.7 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB4721 | 2 | 1 |  |
| 0687-5611 | R: fxd, comp, 560 ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB5611 | 4 | 1 |  |
| 0687-5631 | R: fxd, comp, 56 K ohms $\pm 10 \%, 1 / 2 \mathrm{~W}$ | 01121 | EB5631 | 2 | 1 |  |
| 0690-1221 | R: fxd, comp, 1.2 K ohms $\pm 10 \%$, 1 W | 01121 | GB1221 | 1 | 1 |  |
| 0690-3911 | R: fxd, comp, 390 ohms $\pm 10 \%$, 1W | 01121 | GB3911 | 1 | 1 |  |
| 0727-0100 | R: fxd, dep c, 1 K ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 19701 | DC1/2CR5 obd\# | 1 | 1 |  |

Table 6-2. Replaceable Parts (Cont'd)

| (5ip) Stock No. | Description \# | Mfr. | Mfr. Part No. | TQ | RS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0727-0124 | R: fxd, dep c, 3 K ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 19701 | DC1/2CR5 obd\# | 2 | 1 |  |
| 0727-0131 | R: fxd, dep c, 3920 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 19701 | CD1/2CR5, obd\# | 1. | 1 |  |
| 0727-0341 | R: fxd, dep c, 12 K ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1. | 1 |  |
| 0727-0342 | $\begin{aligned} & \mathrm{R}: ~ f x d, \text { dep } \mathrm{c}, 38.05 \mathrm{~K} \text { ohms } \pm 1 / 2 \% \text {, } \\ & 1 / 2 \mathrm{~W} \end{aligned}$ | 19701 | DC1/2AR5, obd\# | 1. | 1 |  |
| 0727-0346 | R: fxd, dep c, 63.14 K ohms $\pm 1 / 2 \%$ $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1. | 1 |  |
| 0727-0395 | R: fxd, dep c, 316 ohms $\pm 1 / 2 \%, 1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1. | 1 |  |
| 0727-0396 | R: fxd, dep c, 1.194 K ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0397 | R: fxd, dep c, 2.13 K ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0398 | R: fxd, dep c, 3.79 K ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0399 | R: fxd, dep c, 6.73 K ohms $\pm 1 / 2 \%$, 1/2W | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0400 | R: fxd, dep c, 21.36 K ohms $\pm 1 / 2 \%$, 1/2W | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0401 | $\begin{aligned} & \mathrm{R}: ~ f x d, \operatorname{dep} c, 41.46 \mathrm{~K} \text { ohms } \pm 1 / 2 \% \text {, } \\ & 1 / 2 \mathrm{~W} \end{aligned}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0402 | R: fxd, dep c, 46.67 K ohms $\pm 1 / 2 \%$, 1/2W | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0403 | R: fxd, dep c, 52.3 K ohms $\pm 1 / 2 \%$, 1/2W | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0404 | $\begin{aligned} & \text { R: fxd, dep } c, 52.55 \mathrm{~K} \text { ohms } \pm 1 / 2 \% \text {, } \\ & 1 / 2 \mathrm{~W} \end{aligned}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0405 | $\begin{aligned} & \text { R: fxd, dep } \mathrm{c}, 57.46 \mathrm{~K} \text { ohms } \pm 1 / 2 \% \text {, } \\ & 1 / 2 \mathrm{~W} \end{aligned}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0406 | R: fxd, $\operatorname{dep} c, 69.49 \mathrm{~K}$ ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0407 | R: fxd, dep c, 82.09 K ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0408 | $\begin{aligned} & \text { R: fxd, dep c, } 94.2 \mathrm{~K} \text { ohms } \pm 1 / 2 \% \text {, } \\ & 1 / 2 \mathrm{~W} \end{aligned}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0409 | R: fxd, dep c, 142 K ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |
| 0727-0410 | R: fxd, $\operatorname{dep} \mathrm{c}, 256.8 \mathrm{~K}$ ohms $\pm 1 / 2 \%$, $1 / 2 \mathrm{~W}$ | 19701 | DC1/2AR5, obd\# | 1 | 1 |  |

Table 6-2. Replaceable Parts (Cont'd)

| (5p) Stock No. | Description \# | Mfr. | Mfr. Part No. | TQ | RS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0727-0483 | R: fxd, dep c, 318.1 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 28480 | 0727-0483 | 1 | 1 |  |
| 0727-0484 | R: fxd, dep c, 320.1 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 28480 | 0727-0484 | 1 | 1 |  |
| 0727-0485 | R: fxd, dep c, 323.4 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 28480 | 0727-0485 | 1 | 1 |  |
| 0727-0486 | R : fxd, dep c, 329.8 ohms $\pm 1 \%, 1 / 2 \mathrm{~W}$ | 28480 | 0727-0486 | 1 | 1 |  |
| 0758-0003 | $\mathrm{R}: \mathrm{fxd}, \mathrm{mfgl}, 1 \mathrm{~K}$ ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 07115 | C-20, obd\# | 4 | 1 |  |
| 0758-0005 | R: fxd, metallic oxide, 4.7 K ohms $\pm 5 \%, 0.5 \mathrm{~W}$ | 07115 | C-20, obd\# | 1 | 1 |  |
| 0758-0006 | R: fxd, metallic oxide, 10 K ohms $\pm 5 \%, 0.5 \mathrm{~W}$ | 07115 | C-20, obd\# | 1 | 1 |  |
| 0758-0020 | R: fxd, mfgl, 22 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 07115 | C-20, obd\# | 1 | 1 |  |
| 0758-0021 | R: fxd, mfgl, 51 K ohms $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 07115 | C-20, obd\# | 1 | 1 |  |
| 0811-0051 | R: fxd, ww, 200.3 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 05347 | 205RP, obd\# | 2 | 1 |  |
| 0811-0063 | R: fxd, ww, 189 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ | 05347 | 205RP, obd\# | 1 | 1 |  |
| 0811-0064 | R: fxd, ww, 255 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 05347 | 205RP, obd\# | 1 | 1 |  |
| 0811-0065 | R: fxd, ww, 511 ohms $\pm 1 \%, 0.08 \mathrm{~W}$ | 99957 | M3A, obd\# | 2 | 1 |  |
| 0811-0066 | R: fxd, ww, 887 ohms $\pm 1 \%, 0.08 \mathrm{~W}$ | 99957 | M3A, obd\# | 1 | 1 |  |
| 0811-0085 | R: fxd, ww, 202.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0085 | 1 | 1 |  |
| 0811-0086 | R : fxd, ww, 204.3 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0086 | 1 | 1 |  |
| 0811-0087 | R: fxd, ww, 208.8 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0087 | 1 | 1 |  |
| 0811-0088 | R: fxd, ww, 206.6 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0088 | 1 | 1 |  |
| 0811-0089 | R: fxd, ww, 213.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0089 | 1 | 1 |  |
| 0811-0090 | R: fxd, ww, 227.6 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 28480 | 0811-0090 | 1 | 1 |  |
| 0811-0091 | R: fxd, ww, 256 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 28480 | 0811-0091 | 1 | 1 |  |
| 0811-0092 | R: fxd, ww, 262.1 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 28480 | 0811-0092 | 1 | 1 |  |
| 0811-0093 | R: fxd, ww, 265.5 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 28480 | 0811-0093 | 1 | 1 |  |
| 0811-0094 | R: fxd, ww, 190.9 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0094 | 1 | 1 |  |
| 0811-0095 | R: fxd, ww, 194.2 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0095 | 1 | 1 |  |
| 0811-0096 | R: fxd, ww, 200.7 ohms $\pm 0.5 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0096 | 1 | 1 |  |
| 0811-0098 | R: fxd, ww, 258.2 ohms $\pm 0.5 \%, 0.25 \mathrm{~W}$ | 28480 | 0811-0098 | 1 | 1 |  |
| 0811-0099 | R: fxd, ww, 202.5 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0099 | 1 |  |  |
| 0811-0100 | R: fxd, ww, 200.7 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0100 | 1 | 1 |  |
| 0811-0101 | R: fxd, ww, 212.7 ohms $\pm 0.1 \%, 1 / 4 \mathrm{~W}$ | 28480 | 0811-0101 | 1 | 1 |  |

Table 6-2. Replaceable Parts (Cont'd)

| Stock No. | Description \# | Mfr. | Mfr. Part No. | TQ | RS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1205-0002 | Heat sink, transistor | 000II | 3AL635-2R | 2 | 1 |  |
| 1251-0066 | Jack, telephone, for 2 connector plug | 82389 | 2J-1339 | 1 | 1 |  |
| 1251-0148 | Connector, POWER: male, 3 pin | 0000 U | H-1061 1G-3L | 1 | 1 |  |
| 1251-0149 | Connector, female, 6 contact | 02660 | A1-PC6F-1000 | 1 | 1 |  |
| 1400-0084 | Fuseholder: extractor post type | 75915 | 342014 | 1 | 1 |  |
| 1420-0009 | Battery, rechargeable, 1-25AH | 88220 | obd\# | 1 | 1 |  |
| 1450-0048 | Lamp, Ne: NE2H | 08717 | 858-R | 1 | 1 |  |
| 1850-0040 | Transistor, Ge: 2N383 | 94154 | 2N383 | 1 | 1 |  |
| 1850-0064 | Transistor, Ge: 2N1183 | 02735 | 2N1183 | 1 | 1 |  |
| 1850-0065 | Transistor, Ge: 2N1370 | 01295 | 2N1370 | 7 | 7 |  |
| 1851-0017 | Transistor, Ge: 2N1304 | 01295 | 2N1304 | 4 | 4 |  |
| 1854-0003 | Transistor, Si | 07263 | S-3056 | 3 | 3 |  |
| 1901-0024 | Diode, Si | 82647 | G-355-1 | 9 | 9 |  |
| 1901-0025 | Diode, Si: $50 \mathrm{ma} @+1 \mathrm{~V}, 100 \mathrm{PIV}$ | 98925 | CSD2693 | 6 | 6 |  |
| 1902-0017 | Diode, Si: avalanche | 01281 | PS8135 | 2 | 2 |  |
| 1902-0018 | Diode, St: avalanche | 04713 | 1N941 | 1 | 1 |  |
| 1910-0016 | Diode, Ge: 100 ma @ 1V, 60 PIV | 93332 | D2361 | 4 | 4 |  |
| 2100-0182 | ```R: var, comp, lin, 3.3K ohms }\pm10%\mathrm{ , 1/3W``` | 11237 | UPE-70 | 1 | 1 |  |
| 2100-0342 | $R$ : var, concentric <br> Front sect: ww, lin, 10K ohms $\pm 10 \%, 2 \mathrm{~W}$ <br> Rear sect: ww, lin, 800 ohms $\pm 10 \%, 2 \mathrm{~W}$ | 11237 | C2-252 | 1 | 1 |  |
| 2110-0017 | Fuse, cartridge: 0.15 amp | 75915 | 313.150 | 1 | 10 |  |
| 3100-0273 | Switch, rot: 3 sect, 8 pos | 76854 | 213364-K3 | 1 | 1 |  |
| 3100-0370 | Switch, rot: 1 sect, 4 pos | 76834 | obd\# | 1 | 1 |  |
| 3101-0032 | Switch, sl: 4PDT | 42190 | 6613M (spectal) | 1 | 1 |  |
| 3101-0033 | Switch, sl: DPDT | 42190 | 4633 | 1 | 1 |  |
| 8120-0078 | Assy, power cable: smooth black, extra limp, 7.5ft, NEMA plug-in | 70903 | KH-4147 | 1 | 1 |  |

Table 6-2. Replaceable Parts (Cont'd)

| Stock No. | Description \# | Mfr. | Mfr. Part No. | TQ | RS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9100-0141 | Transformer, power | 98734 | 61277 | 1 | 1 |  |
| 9110-0040 | Inductor, audio | 98734 | 1895 | 3 | 1 |  |
| 9120-0065 | Transformer, audio | 98734 | 2-2690 | 2 | 1 |  |
| 9120-0066 | Transformer, audio | 98734 | 2-2695 | 2 | 1 |  |
| 9140-0122 | Coil, var, 2 windings, $9-20 \mu \mathrm{~h}$ each | 09250 | 18-473 | 2 | 1 |  |

## APPENDIX <br> CODE LIST OF MANUFACTURERS (Sheet 1 of 2)

The following code numbers are from the Federal Supply Code for Manufacturers Cataloging Handbooks H4-1 (Name to Code) and $\mathrm{H} 4-2$ (Code to Name) and their latest supplements. The date of revision and the date of the supplements used appear at the bottom of each page. Alphabetical codes have been arbitrarily assigned to suppliers not appearing in the H 4 handbooks.

## CODE

NO. MANUFACTURER
00334 Humidial Co.
ADDRESS

00335 Westrex Corp.
00373 Garlock Packing Co.
Electronic Products' Div.
00656 Aerovox Corp.
00779 Amp, Inc.
00781 Aircraft Radio Corp.
Boonton, N J
00815 Northern Engineering Laboratories, Inc.
Burlington, Wis.
00853 Sangamo Electric Company, Ordill Division (Capacitors) Marion, III. 00866 Goe Engineering Co. Los Angeles, Calif. 00891 Cart E. Holmes Corp. Los Angeles, Calif. 01121 Allen Bradley Co. Milwaukee, Wis. 01255 Litton Industries, Inc. Beverly Hills, Calif. 01281 Pacific Semiconductors, Inc.

Culver City, Calif.
01295 Texas Instruments, Ine. Transistor Products Div. Dallas, Texas 01349 The Alliance Mfg. Co. Alliance, Ohio 01561 Chassi-Trak Corp. Indianapolis, Ind. 01589 Pacific Relays, Inc. Van Nuys, Calif. Rockiord, III. 01961 Pulse Engineering Co. Santa Clara, Calit. 02114 Ferroxcube Corp. of America
02286 Cole Mig. Co. Palo Alto, Calif. 02660 Amphenol-Borg Electronics Corp.

02735 Radio Corp. of America
Semiconductor and Materials Div.
Somerville, N.J.
02771 Yocaline Co. of America, Inc.
02777 Hopkins Engineering Co.
03508 G.E. Semiconductor Products Fernando, Calif. Syracuse, N.Y 03705
03797 Eldema Corp. $\quad$ El Monte, Calif. 03877 Transitron Electronic Corp. Wakefield, Mass. 03888 Pyrofilm Resistor Co. Moristown, N.J. 03954 Air Marine Motors, Inc. Los Angeles, Calif. 04009 Arrow. Hart and Hegeman Elect. Co.

Hartiord, Conn.
04062 Elmenco Products Co. Naw York, N.Y.
$04222 \mathrm{Hi}-\mathrm{Q}$ Division of Aerovox Myrtle Beach, S.C. 04298 Elgin National Watch Co.,

Electronics Division
Burbank, Calif.
04404 Dymec Division of
Palo Alto, Calif.
04651 Sylvania Electric Prods., Inc.
Electronic Tube Div. Mountain View, Calif.
$04713 \begin{aligned} & \text { Motorola, Inc., Semiconductor } \\ & \text { Phod. Div. }\end{aligned}$
04732 Filtron Co., Inc.
Western Division Culver City, Calif.
04773 Automatic Electric Co. Northlake, III.
04796 Sequoia Wire Cable Redwood City, Calif. 04870 P. M. Motor Co. Chicago 44, III. 05006 Twentieth Century Plastics, Inc.
05277 Westinghouse Electric Corp. Angeles, Calif. 05347 Ultronix, Inc. $\begin{gathered}\text { Semator Dept. Youngwood, Pa. } \\ \text { San Mateo, Calif. }\end{gathered}$ 05593 Illumitranic Engineering Co.
05624 Barber Colman Co.
Sunnrvale, Calif.
Rockfor
05729 Metropolitan Telecommunications Corp.
Metro Cap. Div. Brooklyn, N.Y.
05783 Stewart Engineering Co. Santa Cruz. Calif. 06004 The Bassick Co. Bridgeport, Conn. 06136 Ward Leonard Electric LosAngeles, Calif. 08175 Bausch and Lomb Optical Co.
06555 Beede Electrical Instrument Co Rochester, N.Y.
06555 Beede Electrical Instrument Co., Inc.
06812 Torrington Mig. Co., West Div. Van Nuys, Calif.

## CODE


08994 Mel-Rain Indianapolis, Ind.
09026 Babcock Relays, Inc. Costa Mesa, Calif.
09134 Texas Capacitor Co.
Costa Mesa, Calif.
Houston, Texas
09250 Electro Assemblies, Inc.
09569 Mallory Battery Co
Canada, Lłd. Toronto, Ontario, Canada
10214 General Transistor Western Corp.
10411 Ti-Tal, Inc.
Los Angeles, Calif.
10646 Carborundum Co. $\quad \begin{gathered}\text { Berkeley, Calif. }\end{gathered}$
11236 CTS of Berne, Inc. Berne. Ind.
11237 Chicago Telephone of California, Inc.
So. Pasadena, Calif.
11312 Microwave Electronics Corp.
11534 Duncan Electronics, Inc. Salo Alto, Calif.
11719 Denal Santa Ana, Calif.
11711 General Instrument Corporation
11717 Imperial Electronics, Inc. Buena Park, Calis
11870 Melabs, Inc. Palo Alto, Calif.
12697 Clarostat Mfg. Co. Dover N.H
14655 Cornell Dubilier Elec. Corp.
15909 The Daven Co. So. Plainfield, N.J.
16688 De Jur-Amsco Corporation
16758 Long Island City I, N.Y
16758 Delco Radio Div. of G. M. Corp.
Kokomo, Ind
18873 E. I. DuPont and Co., Inc. Wilmington, Del. 19315 Eclipse Pioneer, Div. of

Eclipse Pioneer, Div. of Teterbero, N.J
Bendix Aviation Corp. Ther 19500 Thomas A. Edison Industries.
Div. of McGraw-Edison C.

19701 Electra Manufacturing Co. Kar Orange, N.J. 20183 Electronic Tube Corp. Philadelphia, Pa. 21520 Fansteel Metallurgical Corp.
21335 The Fafnir Bearing Co. No. Chicago, Ill 21964 Fed. Telephone and Radio Corp.
24446 General Electric Co. Schenectady, N.Y.
24455 G.E., Lamp Division
Nela Park, Cleveland, Ohio
24655 General Radio Co. West Concord, Mass. 26462 Grobet File Co. of America, Inc.
26992 Hamilton Watch Co. Carlstadt, N.J. 28480 Hewlett-Packard Co. Palo Alto, Calif. 33173 G.E. Receiving Tube Dept. Owensboro, Ky. 35434 Lectrohm Inc. Chicago. III. 37942 P. R. Mallory \& Co., Inc. Indianapolis, Ind. 39543 Mechanical Industries Prod. Co.

## CODE

NO. MANUFACTURER ADDRESS
40920 Miniature Precision Bearings, Inc.
42190 Muter Co. Keene, N.H.
43990 C. A. Norgren Co. Englewood, Colo.
44655 Ohmite Mig. Co. Skokie, III.
47904 Polaroid Corp.
Cambridge, Mass.
48620 Precision Thermometer and
Inst. Co. Philadelphia, Pa.
49956 Raytheon Company Lexington, Mass. 54294 Shalleross Mfg. Co. Selma, N.C.
55026 Simpson Electric Co. Chicago, III.
55933 Sonotone Corp. Elmsford, N.Y.
55938 Sorenson \& Co., Inc. So. Norwalk, Conn. 56137 Spaulding Fibre Co., Inc. Tonawanda, N.Y. 56289 Spraque Electric Co. North Adams, Mass. 59446 Telex. Inc. St. Paul, Minn
61775 Union Switch and Signal, Div, of
Westinghouse Air Brake Co. Swissvale, Pa.
62119 Universal Electric Co. Owosso, Mich.
64959 Western Electric Co., Inc. New York, N.Y.
65092 Weston Inst. Div. of Daystrom, Inc.
Newark, N.J.
66295 Wittek Manufacturing Co. Chicago 23. ili. 66346 Wollensak Optical Co. Rochester, N.Y. 70276 Allen Mig. Co. Hartford, Conn 70309 Allied Contral Co., Inc. New York, N,Y, 70485 Atlantic India Rubber Works, Inc. Chicago, III
70563 Amperite Co., Inc. Chicago, III.
70903 Belden Mfg. Co. Chicago, III.

70998 Bird Electronic Corp. Cleveland, Ohio 71002 Birnbach Radio Co. New York, N.Y. 71041 Boston Gear Works Div, of Murray Co. of Texas

Quincy, Mass.
71218 Bud Radio Inc. Cleveland, Ohio
7128 ( Camloc Fastener Corp. Paramus, N.J
71313 Allen D. Cardwell Electronic
Prod. Corp.
$71400 \begin{gathered}\text { Bussmann Fuse Div. of McGraw- } \\ \text { Edison Co. Louis, Mo }\end{gathered}$
Plainville, Conn.

71450 CTS Corp Elkhart
71468 Cannon Electric Co. Los Angeles, Calif.
71471 Cinema Engineering Co. Burbank, Calif
71482 C. P. Clare \& Co.
Chicago, III.
71528 Standard-Thomson Corp.,
Clifford Mig. Co. Div. Waltham, Miass
71590 Centralab Div. of Globe Union Inc.
Milwaukee, Wis
71700 The Cornish Wire Co. New York, N.Y
71744 Chicago Miniature Lamp Works
Chicago, III.
71753 A. O. Smith Corp., Crowley Div.
West Örange. N.J.
71785 Cinch Mig. Corp. Chicago, III.
71984 Dow Corning Corp. Midland, Mich
72136 Electro Motive Mfg. Co., Inc.
Willimantic, Conn
72354 John E. Fast \& Co. Chicago, III
72619 Dialight Corp. Brooklyn, N.Y
72856 General Ceramics Corp. Keasbey, N.J.
72758 Girard-Hopkins
Oakland, Calif.
72765 Drake Mig. Co.
Chicago, III.
72825 Hugh H. Eby Ine. Philadelphia, Pa.
72928 Gudeman Co. Chicago, III.
72964 Robert M. Hadiey Co. Los Angeles, Calif.
$\begin{array}{llr}72982 & \text { Erie Resisfor Corp. } & \text { Erie, Pa } \\ 73061 & \text { Hansen Mfg. Co., Inc. } & \text { Princeton, Ind }\end{array}$
Princeton, Ind.
7313 B Helipot Div. of Beckman
Fullerton, Calif.
73293 Hughes Products Division of
73445 Amperex Electronic Co Divor
North American Phillips Co.. Inc.
73506 Bradley Semiconductor Corp. Hamden, Conn
73559 Carling Electric. Inc. Hartford, Conn.
73682 George K. Garrett Co., Inc.
Philadelphia, Pa.

From: F.S.C. Handbook Supplements
H4-1 Dated: June 1962
H4-2 Dated: March 1962

APPENDIX
CODE LIST OF MANUFACTURERS (Sheet 2 of 2)

CODE
NO. MANUFACTURER
73734 Federal Screw Products Co. 73743 Fischer Special Míg. Co. 73793 The General Industries Co. 73905 Jennings Radio Mfg. Co. $74455 \mathrm{~J} . \mathrm{H}$. Winns, and Sons 74861 Industrial Condenser Corp. 74868 R.F. Products Division of Amphenol-

Borg Electronics Corp.

## 74970 E. F. Johnson Co

75173 Jones, Howard B., Divisio of Cinch Mig. Corp.
75378 James Knights Co.
75382 Kulka Electric Corporation 75818 Lenz Electric Mfg. Co.
75915 Littelfuse Inc.
76005 Lord Mfg. Co.
76433 Micamold Electronic Mfg. Corp.
76487 James Millen Mfg. Co., Inc. Malden, Mass. 76493 J Willer Co Los Angeles, Calif, 76530 Monadnock Mills

San Leandro, Calif.
76545 Mueller Electric Co. Cleveland, Ohio
76854 Oak Manufacturing Co. Crystal Lake, III.
$77068 \begin{gathered}\text { Bendix Pacific Division of } \\ \text { Bendix Corp. }\end{gathered}$ No. Hollywood, Calif.
77221 Phaostron Instrument and
Electronic Co. South Pasadena, Calif.
77252 Philadelphia Steel and Wire Corp.
Philadelphia, Pa.
77342 Potter and Brumfiald, Div. of American 77630 Radio Condenser Co. Princeton, ind.
77638 Radio Receptor Co., Inc. Brooklyn, N.Y.
77764 Resistance Products Co.
Harrisburg, Pa.
78189 Shakeproof Division of Illinois Tool Works

Elgin, III.
78283 Signal Indicator Corp. New York, N.Y. 78471 Tilley Mfg. Co. San Francisco, Calif.
78488 Stackpole Carbon Co.
78553 Tinnerman Products, Inc. St. Marys, Pa.

78790 Transformer Engineers
78947 Ucinite Co.
Cleveland, Ohio
Pasadena, Calif.
79142 Veeder Root, Inc.
79251 Wenco Mfg. Co.
79727 Continental-Wirt Electronics Corp.
79963 Tick Míladelphia, Pa.
80031 Mepco Division of
New Rochelle, N.Y.
Sassions Clock Co.
Morristown, N.J.
80120 Schnizer Alloy Products Elizabeth, N.J.
80130 Times Facsimile Corp.
80131 Electronic Industries Association Any brand tube mesting ElA
80207 Unimax Switch, Div, of W. L. Maxson Corp.

80248 Oxford Elactric Corp. Chicago. M.
80294 Bourns Laboratories, Inc. Riverside, Calif.
B0411 Acro Div. of Robertshaw Fulton Controls Co.
80486 All Star Products Inc.
80583 Hammerlund Co., Inc. 81030 Stevens, Arnold, Co., inc.
81030 International Instruments, Inc.
Now Haven, Conn. Inc.
Norwalk, Conn.
81415 Wilkor Products, Inc. Clevaland, Ohio
81453 Raytheon Mig. Co., Industrial
Tube Operations
81483 International Rectifier Corp.
El Segundo, Calif.
81860 Barry Controls, Ine. Watertown, Mass.
B2042 Carter Parts Co.
82142 Jeffers Electronics Division of Speer Carbon Co.
82170 Allen B. DuMont Labs., Inc.
82209 Maguire Industries, Inc.
82219 Sylvania Electric Prod. Inc., Electronic Tube Div.
82376 Astron Co.
82389 Switcheraff, Inc.

CODE
NO. MANUFACTURER
82647 Metais and Controls, Inc., Div. of
Texas listruments, 'Inc.,
Spencer Prods.
ADDRESS

82866 Research Products. Corp Attleboro. Mass. 82877 Rotron Manufacturing Co., Inc.

Madison, Wis.
oodstock, N.Y
82893 Vector Electronic Co. Glendale, Calif
83053 Western Washer Mfr. Co. Los Angeles, Calif.
8 305 B Carr Fastener Co. Cambridge, Mass.
83086 New Hampshire Ball Bearing, Inc.
Peterborough, N.H.
83125 Pyramid Electric Co. Darlington, S.C.
83148 Electro Cords Co. Los Angeles, Calif.
83186 Victory Engineering Corp. Union, N.J.
83298 Bendix Corp., Red Bank Div. Red Bank, N.J. 83330 Smith, Herman H., Inc. Brooklyn, N.Y. 83501 Gavitl Wire and Cable Co.
Div. of Amerace Corp. Brookfield, Mass
$83594 \begin{gathered}\text { Burroughs Corp.i } \\ \text { Electronic Tube Div. Plainfleld, N.J }\end{gathered}$
83777 Model Eng. and Mfg., Inc. Huntington, Ind
83821 Loyd Scruggs Co. Festus, Mo.
84171 Arco Electronics, Inc. New York, N.Y.
84396 A. J. Glesener Co., Inc.
San Francisco. Calif
84411 Good All Electric Mfg. Co. Ogallala, Neb.
84970 Sarkes Tarzian, Inc. Bloomingłon, Ind. 85454 Boonton Molding Company Boonton, N.J. 95471 A. 日. Boyd Co. San Francisco, Calif 85474 R. M. Bracamonte \& Co.
85660 Koiled Kords, Inc. New Haven, Conn. 85911 Seamless Rubber Co. Chicago, III.
86197 Clifton Precision Products
86684 Radio Corp. of America, RCA
Electron Tube Div. Harrison, N.J. 87216 Philco Corp. (Lansdale Division)
87473 Western Fibrous Glass Products Co.
88140 Cutier-Hammer, Inc. San Francisco, Calif.
88220 Gould-National Batferies, Inc. St. Paul, Minn
89473 General Electric Distributing Corp.
Schenectady, N.Y 89636 Carter Parts Div. of Economy Baler Co.
89665 United Transformer Co. Chicago, III.
90179 U.S. Rubber Co., Mechanical
Goods Div
Passaic, N.J.
90970 Bearing Enginearing Co. San Francisco, Calif. 91260 Connor Spring Mig. Co. San Francisco, Calif. 91345 Miller Dial \& Nameplate Co.

91418 Radio Materials Co
91506 Augat Brothers,'Ine.
91637 Dale Electronics, Inc.
91662 Elco Corp.
91737 Gremar Mig. Co., Ine
37 Gremar Mfg. Co., Inc Wakefield Mass
91827 KFDevelopment Co. Redwood City, Calif.
91921 Minneapolis-Honeywell Regulator Co.,
92196 Micro-Switch Division
93332 Sylvania Electric Prod. Ine.,
93369 Robbins and Myers, Inc. Woburn, Mass. 9369 Robbins and Myers, Inc. 93410 Stevens Mfg. Co., Inc. 93983 Insuline-Van Norman Ind., Inc 94144 Raytheon Mfg. Co. Industrial Compor, N.H 94144 Raytheon Mfg. Co., Industrial Components
uincy, Mass
94145 Raytheon Mfg. Co., Semiconductor Div. $\begin{gathered}\text { California Street } \\ \text { Clant } \\ \text { Newton, Mass }\end{gathered}$ 94148 Scientific Radio Products, Inc

94154 Tung-Sol Electric, Inc.
Loveland, Colo.
Newark, N.J.
94197 Curtiss-Wright CorP., East Paterson, N.J.
94310 Tru Ohm Prod. Div. of Modal
94310 Tru Engin Prod. Div, of Model Chicago, III
946 B2 Worcester Pressed Aluminum Corp.
Worcester, Mass
95238 Allies Products Corp. Miami, Fla
95238 Continental Connector Corp. Woodside, N.Y.
95263 Leecraft Mig. Co., Inc. New York, N.Y.
95264 Lerco Electronics, Inc. Burbank, Calif.

## CODE

## NO. MANUFACTURER

ADDRESS
95265 National Coil Co
95275 Vitramon, Inc.
95354 Methode Mfq. Co
95987 Weckesser Co.
96067 Huggins Laboratories
Sheridan, Wyo
Bridgeport, Conn
Chicago. III.
Chicago, III.
$96095 \mathrm{Hi}-\mathrm{O}$ Division of Aerovox
Sunnyvale, Calif.
96256 Thordarson-Meissner Div. of
Maguire Industries, Inc. Mt. Carmel, III
96296 Solar Manufacturing Co. Los Angeles, Calif.
96330 Carlton Screw Co. Chicago, III.
96341 Microwave Associates, Inc. Burlington, Mass.
96501 Excel Transformer Co. Oakland, Calif.
97464 Industrial Retaining Ring Co. Irvington, N.J.
97539 Automatic and Precision
Mig. Co.
Yonkers, N.Y
97966 CBS Electronics,
Danvers, Mass.
98141 Axel Brothers Inc.
98220 Francis L. Mosley
98278 Microdot, Inc.
98291 Sealectro Corp.
98405 Carad Corp.
98734 Palo Alto Engineering Co., Inc.

Jamaica, N.Y. Pasadena, Calif. So. Pasadena, Calif Mamaroneck, N.Y Redwood City, Calif.

Palo Alto, Calif
98925 Clevife Transistor Prod Div. of Clevite Corp.

Mineola, N.Y

98978 International Electronic
Waltham, Mass Research Corp.

Burbank, Calif
99109 Columbia Technical Corp. New York, N.Y
94313 Varian Associates
99515 Marshall Industries, Electron Products Division Palo Alto, Calif

99707 Control Switch Division, Controls Co
El Segundo, Calif East Aurora, N.Y
99848 Wileo Corporation Indianapolis, Ind
99934 Renbrandt. Inc.
Indianapolis, Ind.
99942 Hoffman Semiconductor Div. of
9995 Hoffman Electronics Corp.
Evanston, III.
99957 Technology Instrument Corp.
Newbury Park, Calif.
THE FOLLOWING H-P VENDORS HAVE NO NUM BER ASSIGNED IN THE LAIEST SUPPLEMENT TO HE FEDERAL SUPPLY CODE FOR MANUFACTURERS HAND8OOK.
0000 F Malco Tool and Die Los Angeles, Calif.
00001 Telefunken (c/o American Elite)

New York, N.Y.
0000 M Western Coil Div. of Automatic
Ind., Ine. Redwood City, Calif.
0000 N Nahm-Bros. Spring Co. San Leandro, Calif.
0000 P Ty-Car Mig. Co., Inc. Holliston, Mass.
0000 T Texas Instruments, Inc,
Metals and Controls Div.
Versailles, Ky.
0000 U Tower Mfg. Corp. Providence, R.I.
0000 W Webster Electronics Co. Inc.
$0000 \times$ Spruce Pine Mica Co. Spruce Pine, N.Y
0000 Y Midland Mig. Co. Inc. Kansas City, Kans.
$0000 Z$ Willow Leather Products Corp. Newark, N.J.
000 A A British Radio Electronics Lid.
Washington, D.C.
000 B B Precision Instrument Components Co.
00 C C Computer Diode Corp Van Nuys, Call
000EE A. Williams Manufacturing Co.
n Jose, Calif.
000FF Carmichasl Corrugated Specialties
Richmond, Calif
000 GG Goshen Die Cutting Service Goshen, Ind. 000 H H Rubbercrafł Corp. Torrance, Calif.
00011 Birtcher Corporation, Industrial
Division Monterey Park, Calif. 000 KK Amatom Now Rochalle, N.Y
OOOLL Avary Label
Monrovia, Calif
000 M M Rubber Eng. ${ }^{2}$
Development
Hayward, Calif.
000 N N A "N" D Manufacturing Co.
San Jose 27, Calif
000 PP Atohm Electronics, Sun Valley, Calif
Oakland, Calif
R Radio Industries Watch Co Des Plaines, ill
$0005 S$ Control of Elgin Watch Co. Burbank, Calif
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00015-28
Revised: 4 September 1962
H4-2 Dated: March 1962

## WARRANTY

All our products are warranted against defects in materials and workmanship for one year from the date of shipment. Our obligation is limited to repairing or replacing products (except tubes) which prove to be defective during the warranty period. We are not liable for consequential damages.

For assistance of any kind, including help with instruments under warranty, contact your authorized Sales Representative for instructions. Give full details of the difficulty and include the instrument model and serial numbers. Service data or shipping instructions will be promptly sent to you. There will be no charge for repair of instruments under warranty, except transportation charges. Estimates of charges for non-warranty or other service work will always be supplied, if requested, before work begins.

## CLAIM FOR DAMAGE IN SHIPMENT

Your instrument should be inspected and tested as soon as it is received. The instrument is insured for safe delivery. If the instrument is damaged in any way or fails to operate properly, file a claim with the carrier or, if insured separately, with the insurance company.

## SHIPPING

On receipt of shipping instructions, forward the instrument prepaid to the destination indicated. You may use the original shipping carton or any strong container. Wrap the instrument in heavy paper or a plastic bag and surround it with three or four inches of shock-absorbing material to cushion it firmly and prevent movement inside the container.

## GENERAL

Your authorized Sales Representative is ready to assist you in any situation, and you are always welcome to get directly in touch with Hewlett-Packard service departments:

## CUSTOMER SERVICE

Hewlett-Packard Company
395 Page Mill Road
Palo Alto, California, U.S.A.
Telephone: (415) 326-1755
TWX No. PAL AL 117-U
Cable: "HEWPACK"

## OR (In Western Europe)

Hewlett-Packard S.A.
54-54bis Route Des Acacias
Geneva, Switzerland
Telephone: (022) 42. 81. 50
Cable: "HEWPACKSA"

